

Unit 4

Digital Filters

Differential Equation for most practical cases -

$$\sum_{k=0}^{m-1} a_k y(n-k) = \sum_{k=0}^{N-1} b_k x(n-k)$$

$$a_0 y(n) + \sum_{k=1}^{m-1} a_k y(n-k) = \sum_{k=0}^{N-1} b_k x(n-k)$$

$$y(n) = - \sum_{k=1}^{m-1} a_k y(n-k) + \sum_{k=0}^{N-1} b_k x(n-k)$$

• Finite Impulse Response (FIR) -

$$a_k = 0$$

$$1 \leq k \leq m-1$$

$$y(n) = \sum_{k=0}^{N-1} b_k x(n-k)$$

This will be a non-recursive system because there's no feedback.

length of $h(n)$ will be of finite duration. 83

This system is also called moving average system, because the present output depends on the weighted sum of inputs.

$$Y(z) = \sum_{k=0}^{N-1} b_k \cdot z^{-k} \cdot X(z)$$

$$H(z) = \sum_{k=0}^{N-1} b_k \cdot z^{-k}$$

This system is also called as All Zero System.

because we get the poles at $z=0$, and the magnitude response will depend only on the zeroes and not on poles. The system is always stable.

• IR (Infinite Response) :-

This is also known as All Pole System also Auto Regressive systems.

$$y(n) = - \sum_{k=1}^{m-1} a_k \cdot y(n-k) + b_0 \cdot x(n)$$

Find its Z transform;

$$Y(z) = - \sum_{k=1}^{m-1} a_k \cdot z^{-k} \cdot Y(z) + b_0 X(z)$$

$$H(z) = \frac{b_0}{1 + \sum_{k=1}^{m-1} a_k \cdot z^{-k}}$$

This IR system is called a Recursive system.

The duration of impulse response is infinite. 84

This is called as Auto Regressive system. because the output depends on its previous values.

This is called All pole system because poles can exist anywhere but zeroes lies only on $z=0$.

They are not necessarily stable.

• Pole zero on Auto Regressive Moving Average

System -

$$y(n) = - \sum_{k=1}^{m-1} a_k \cdot y(n-k) + \sum_{k=0}^{N-1} b_k \cdot x(n-k)$$

$$Y(z) = - \sum_{k=1}^{m-1} a_k \cdot z^{-k} \cdot Y(z) + \sum_{k=0}^{N-1} b_k \cdot X(z) z^{-k}$$

$$Y(z) + \sum_{k=1}^{m-1} a_k \cdot z^{-k} \cdot Y(z) = \sum_{k=0}^{N-1} b_k \cdot z^{-k} \cdot X(z)$$

$$Y(z) \left[1 + \sum_{k=1}^{m-1} a_k \cdot z^{-k} \right] = \sum_{k=0}^{N-1} b_k \cdot z^{-k} \cdot X(z)$$

$$\frac{Y(z)}{X(z)} = \frac{\sum_{k=0}^{N-1} b_k \cdot z^{-k}}{\left(1 + \sum_{k=1}^{m-1} a_k \cdot z^{-k} \right)}$$

This will be a Recursive system.

• FIR System :-

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$$H(z) = \sum_{k=0}^{m-1} b_k \cdot z^{-k}$$

$$H(z) = b_0 z^{-0} + b_1 z^{-1} + b_2 z^{-2} + b_3 z^{-3} + b_4 z^{-4} + \dots \\ \dots + b_{m-1} z^{-(m-1)}$$

$$Y(z) = [b_0 z^{-0} + b_1 z^{-1} + \dots + b_{m-1} z^{-(m-1)}] \cdot X(z)$$

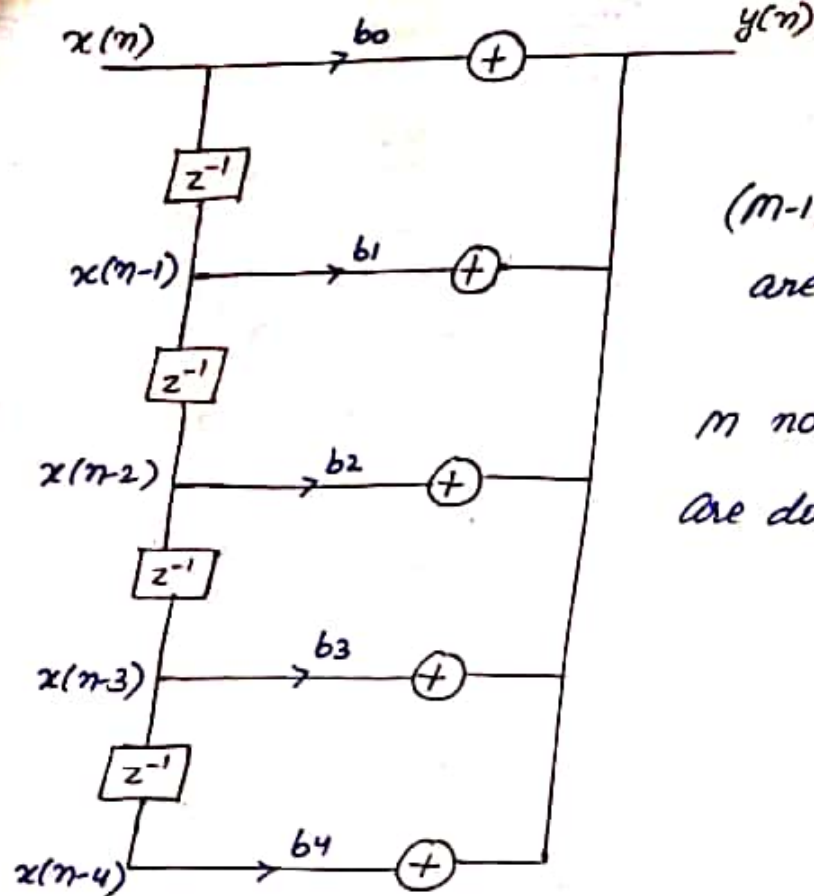
$$y(n) = b_0 x(n) + b_1 x(n-1) + b_2 x(n-2) + \dots \\ \dots + b_{m-1} x(n-(m-1))$$

length of the filter is m and the order of the filter is $(m-1)$.

• Direct form or Tapped Delay in line or Transversal :-

$$m = 5$$

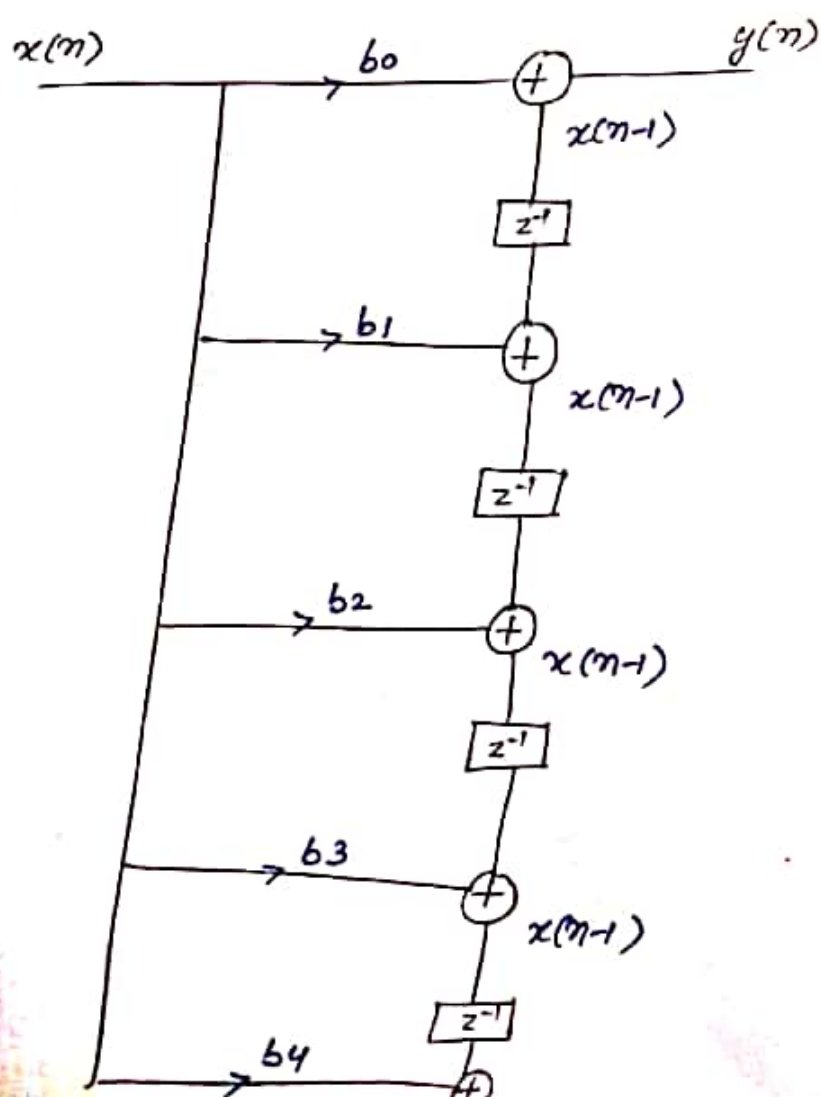
$$y(n) = b_0 x(n) + b_1 x(n-1) + b_2 x(n-2) + \dots \\ \dots + b_4 x(n-4)$$



$(m-1)$ no. of delay lines are used.

m no. of multiplications are done.

• Transposed Direct Form :-



Ques. Consider the system with function,

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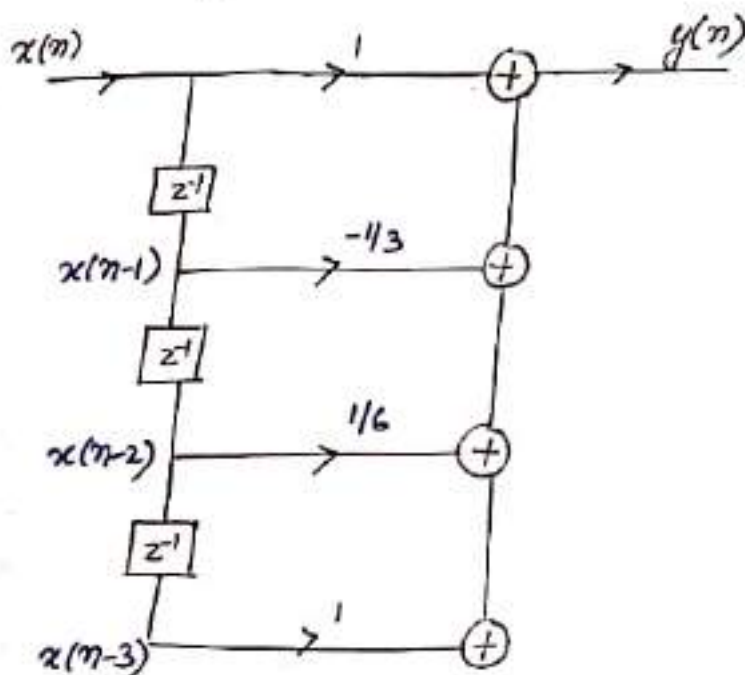
$$H(z) = 1 - \frac{1}{3}z^{-1} + \frac{1}{6}z^{-2} + z^{-3}$$

Order = 3

length of the system = 4

That means, 3 delay lines are used and 4 multipliers are needed.

$$Y(z) = \left[1 - \frac{1}{3}z^{-1} + \frac{1}{6}z^{-2} + z^{-3} \right] \cdot X(z)$$



• Cascade form Structure :-

$$H(z) = b_0 + b_1 z^{-1} + b_2 z^{-2} + b_3 z^{-3} + \dots + b_{m-1} z^{-(m-1)}$$

$$H(z) = b_0 \left[1 + \frac{b_1}{b_0} z^{-1} + \frac{b_2}{b_0} z^{-2} + \frac{b_3}{b_0} z^{-3} + \dots + \frac{b_{m-1}}{b_0} z^{-(m-1)} \right]$$

$$H(z) = \begin{cases} b_0 \prod_{k=1}^{(m-1)/2} [1 + \beta_{1k} z^{-1} + \beta_{2k} z^{-2}] & ; m \text{ is odd} \\ b_0 (1 + b_{10} z^{-1}) \prod_{k=1}^{(m-2)/2} [1 + \beta_{1k} z^{-1} + \beta_{2k} z^{-2}] & ; m \text{ is even} \end{cases}$$

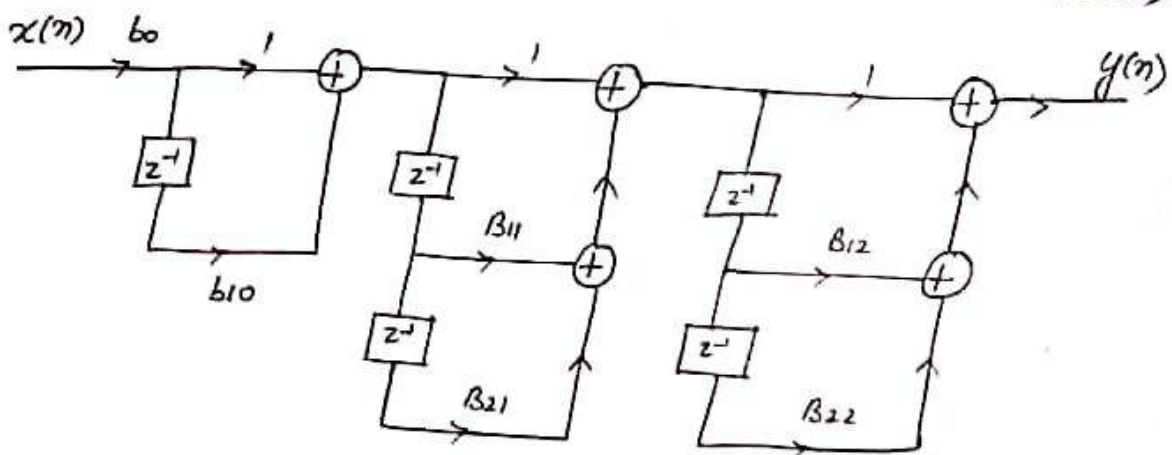
Example :-

$$m = 6$$

$$H(z) = b_0 (1 + b_{10} z^{-1}) \prod_{k=1}^{(6-2)/2} [1 + \beta_{1k} z^{-1} + \beta_{2k} z^{-2}]$$

$$= b_0 (1 + b_{10} z^{-1}) \prod_{k=1}^2 [1 + \beta_{1k} z^{-1} + \beta_{2k} z^{-2}]$$

$$H(z) = b_0 (1 + b_{10} z^{-1}) (1 + \beta_{11} z^{-1} + \beta_{21} z^{-2}) (1 + \beta_{12} z^{-1} + \beta_{22} z^{-2})$$



This format is used when the order of the filter is very high.

Transpose cascaded form will also be similar to the Transpose direct form.

(only z^{-1} will be shifted)

Ques: Obtain the cascaded form of the given filter - 89

$$H(z) = 1 + \frac{6}{5}z^{-1} + \frac{7}{5}z^{-2} + \frac{26}{25}z^{-3} + \frac{1}{5}z^{-4}$$

$m = 5$ i.e. odd.

Hence,

$$H(z) = b_0 \prod_{k=1}^{(m-1)/2} [1 + \beta_{1k}z^{-1} + \beta_{2k}z^{-2}]$$

i.e. we obtain two factors.

$$H(z) = b_0 \prod_{k=1}^2 [1 + \beta_{1k}z^{-1} + \beta_{2k}z^{-2}]$$

$$= b_0 (1 + \beta_{11}z^{-1} + \beta_{21}z^{-2}) (1 + \beta_{12}z^{-1} + \beta_{22}z^{-1})$$

$$= (b_0 + b_0\beta_{11}z^{-1} + b_0\beta_{21}z^{-2}) \cdot (1 + \beta_{12}z^{-1} + \beta_{22}z^{-1})$$

$$= b_0 + b_0\beta_{12}z^{-1} + b_0\beta_{22}z^{-2} + b_0\beta_{11}z^{-1} + \beta_{11}\beta_{12}b_0z^{-2}$$

$$+ b_0\beta_{11}\beta_{22}z^{-3} + b_0\beta_{21}z^{-2} + b_0\beta_{21}\beta_{12}z^{-3} +$$

$$b_0\beta_{21}\beta_{22}z^{-4}$$

$$= b_0 + (\beta_{11} + \beta_{12})b_0z^{-1} + (\beta_{22} + \beta_{11}\beta_{12} + \beta_{21})b_0z^{-2}$$

$$+ (\beta_{11}\beta_{22} + \beta_{21}\beta_{12})b_0z^{-3} + \beta_{21}\beta_{22}b_0z^{-4}$$

On comparing:

$$b_0 = 1$$

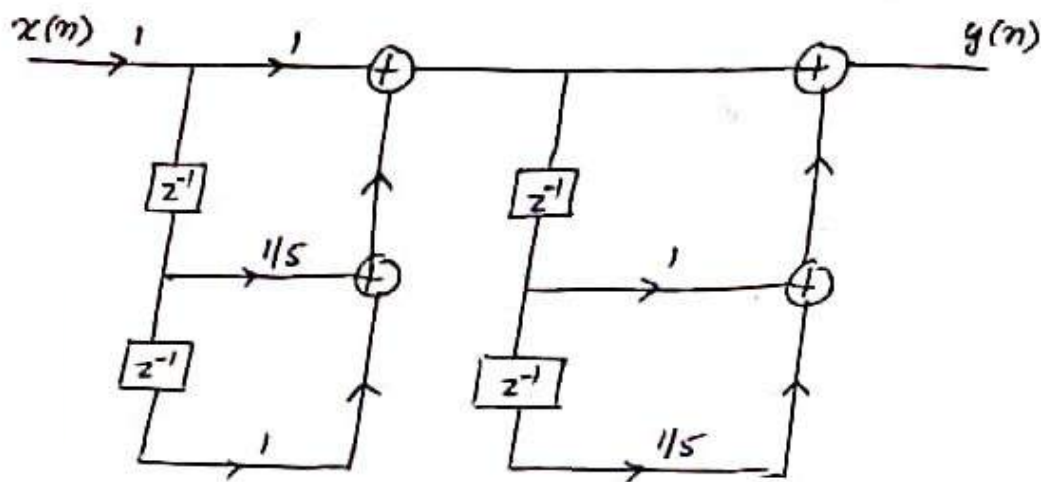
$$\beta_{11} + \beta_{12} = \frac{6}{5}$$

$$\beta_{11}\beta_{22} + \beta_{21}\beta_{12} = \frac{26}{25}$$

$$\beta_{22} + \beta_{11}\beta_{12} + \beta_{21} = \frac{7}{5}$$

$$= 1 \left[1 + \frac{1}{5} z^{-1} + z^{-2} \right] \cdot \left[1 + z^{-1} + \frac{1}{5} z^{-2} \right]$$

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• Linear Phase Structure:-

It is desirable for linear phase which has a linear phase response.

$$\angle H(e^{j\omega}) = \beta - \alpha \omega \quad -\pi < \omega < \pi$$

When $\beta = 0$,

we obtain a symmetric condition,

$$h(n) = h(m-1-n)$$

When $\beta = \pm \frac{\pi}{2}$,

we obtain an asymmetric condition,

$$h(n) = -h(m-1-n)$$

If m is odd, we obtain $\left(\frac{m+1}{2}\right)$ no. of multipliers.

If m is even, the multipliers are reduced to $\frac{m}{2}$.

Q. $m=6$ and $\beta=0$

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$$H(z) = b_0 + b_1 z^{-1} + b_2 z^{-2} + b_3 z^{-3} + b_4 z^{-4} + b_5 z^{-5}$$

$$H(z) = \sum_{k=0}^{m-1} a_k z^{-k} = \sum_{k=0}^{m-1} h(n) z^{-k}$$

$$H(z) = h(0) + h(1) z^{-1} + h(2) z^{-2} + h(3) z^{-3} + h(4) z^{-4} + h(5) z^{-5}$$

$$h(n) = h(1-m-n)$$

$$h(0) = h(5)$$

$$h(1) = h(4)$$

$$h(2) = h(3)$$

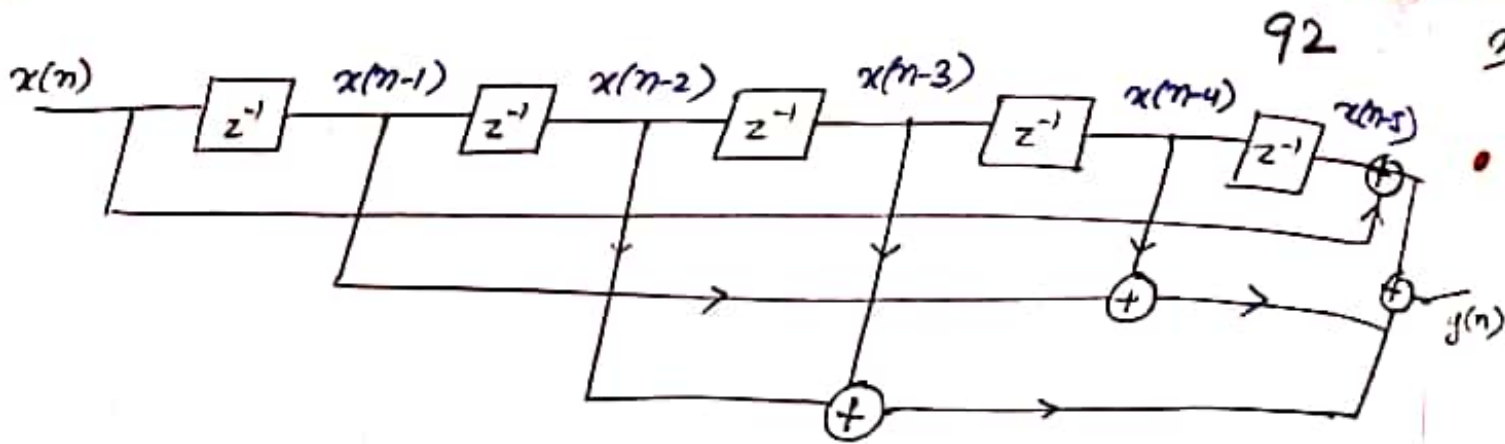
\therefore

$$H(z) = h(0) [1 + z^{-5}] + h(1) [z^{-1} + z^{-4}] +$$

$$h(2) [z^{-2} + z^{-3}]$$

$$Y(z) = [b_0 (1 + z^{-5}) + b_1 (z^{-1} + z^{-4}) + b_2 (z^{-2} + z^{-3})] X(z)$$

$$y(n) = b_0 [x(n) + x(n-5)] + b_1 [x(n-1) + x(n-4)] + b_2 [x(n-2) + x(n-3)]$$



Here, instead of 6 we are using just half
3 multipliers. The circuit becomes simple.

Frequency Sampling -

$$H(z) = \sum_{n=0}^{m-1} h(n) \cdot z^{-n}$$

$$= \sum_{n=0}^{m-1} \left[\frac{1}{M} \sum_{k=0}^{M-1} H(k) e^{-j \frac{2\pi}{M} k n} \right] \cdot z^{-n}$$

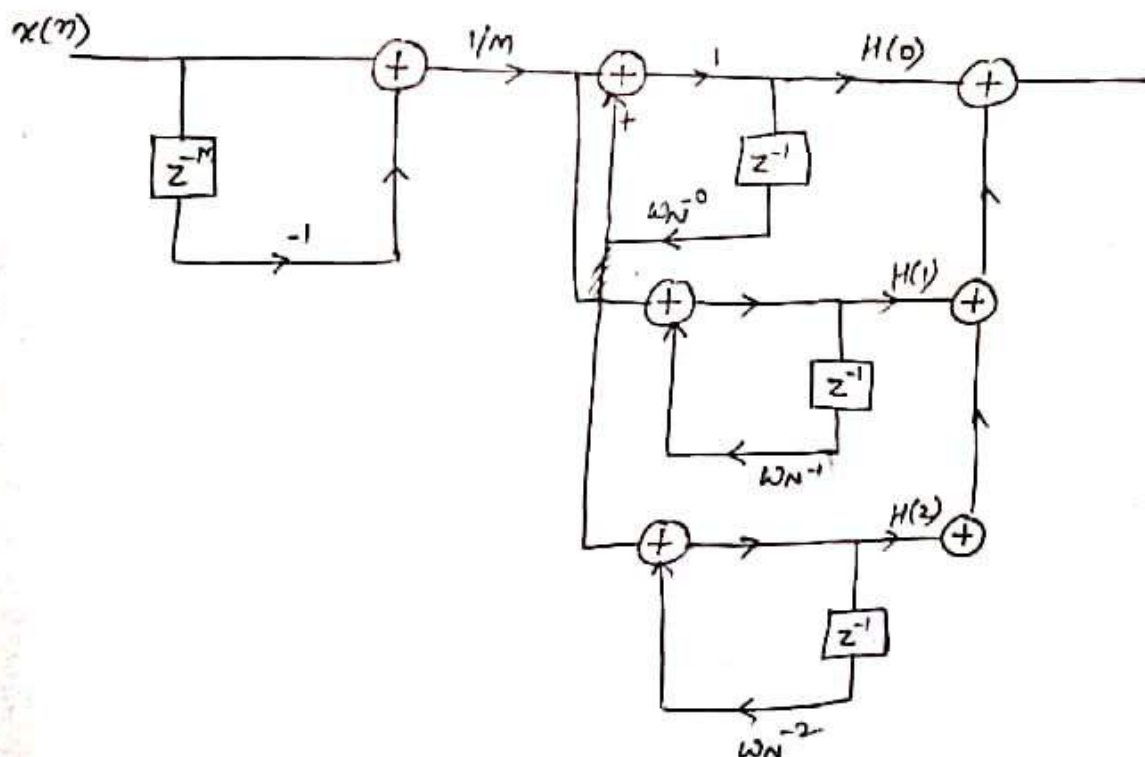
$$= \frac{1}{M} \sum_{k=0}^{M-1} H(k) \cdot \sum_{n=0}^{m-1} e^{j \frac{2\pi}{M} k n} \cdot z^{-n}$$

$$= \frac{1}{M} \sum_{k=0}^{M-1} H(k) \cdot \left[1 + e^{j \frac{2\pi}{M} k} z^{-1} + e^{j \frac{2\pi}{M} 2k} z^{-2} + \dots + e^{j \frac{2\pi}{M} (m-1)k} z^{-(m-1)} \right]$$

= forming a finite GP

$$\underbrace{\frac{1-z^{-m}}{M}}_{H_1(z)} \cdot \sum_{k=0}^{M-1} \underbrace{\frac{H(k)}{1-e^{j \frac{2\pi}{M} k} z^{-1}}}_{H_2(z)}$$

$$\frac{q(s)}{1-q(s) \cdot H(s)}$$



$$H(k) = H^*(M-k)$$

$$H^*(k) = H(M-k)$$

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$$e^{j\frac{2\pi}{m}(m-k)} = e^{-j\frac{2\pi}{m}k}$$

$$H(z) = \frac{1-z^{-m}}{m} \underbrace{\sum_{k=0}^{m-1} \frac{H(k)}{1-e^{j\frac{2\pi}{m}k}z^{-1}}}_{H_2(z)}$$

put $m=3$ in $H_2(z)$.

$$\sum_{k=0}^{m-1} \frac{H(k)}{1-e^{j\frac{2\pi}{m}k}z^{-1}} = \sum_{k=0}^2 \frac{H(k)}{1-e^{j\frac{2\pi}{3}k}z^{-1}}$$

$$H_2(z) = \frac{H(0)}{1-e^{j\frac{2\pi}{3}(0)}z^{-1}} + \frac{H(1)}{1-e^{j\frac{2\pi}{3}(1)}z^{-1}} + \frac{H(2)}{1-e^{j\frac{2\pi}{3}(2)}z^{-1}}$$

$$\text{for } m=3, \\ k=2$$

$$H(2) = H^*(3-2)$$

$$H(2) = H^*(1)$$

Also;

$$e^{j\frac{2\pi}{m}(m-k)} \text{ put } m=3 \\ k=1$$

$$= e^{-j\frac{2\pi}{m}k}$$

$$= e^{-j\frac{2\pi}{3}(1)}$$

6.

$$H_2(z) = \frac{H(0)}{1 - e^{j\frac{2\pi}{3}(0)} z^{-1}} + \frac{H(1)}{1 - e^{j\frac{2\pi}{3}} z^{-1}} + \frac{H^*(1)}{1 - e^{-j\frac{2\pi}{3}} z^{-1}}$$

$$H_2(z) = \begin{cases} \sum_{k=1}^{\frac{m-1}{2}} \left[\frac{H(k)}{1 - e^{j\frac{2\pi}{m}k} z^{-1}} + \frac{H^*(k)}{1 - e^{-j\frac{2\pi}{m}k} z^{-1}} \right] + \frac{H(0)}{1 - z^{-1}} & \text{for } m \text{ is odd.} \\ \sum_{k=1}^{\frac{m-1}{2}} \left[\frac{H(k)}{1 - e^{j\frac{2\pi}{m}k} z^{-1}} + \frac{H^*(k)}{1 - e^{-j\frac{2\pi}{m}k} z^{-1}} \right] + \frac{H(0)}{1 - z^{-1}} + \frac{H(m/2)}{1 - z^{-1}} & \text{for } m \text{ is even.} \end{cases}$$

To remove the complex terms;

$$\frac{H(k)}{1 - e^{j\frac{2\pi}{m}k} z^{-1}} + \frac{H^*(k)}{1 - e^{-j\frac{2\pi}{m}k} z^{-1}}$$

On cross multiplying them;

$$\begin{aligned} &= \frac{H(k) [1 - e^{-j\frac{2\pi}{m}k} z^{-1}] + H^*(k) [1 - e^{j\frac{2\pi}{m}k} z^{-1}]}{[1 - e^{j\frac{2\pi}{m}k} z^{-1}] [1 - e^{-j\frac{2\pi}{m}k} z^{-1}]} \\ &= \frac{H(k) - H(k) e^{-j\frac{2\pi}{m}k} z^{-1} + H^*(k) - H^*(k) e^{j\frac{2\pi}{m}k} z^{-1}}{1 - e^{-j\frac{2\pi}{m}k} z^{-1} - e^{j\frac{2\pi}{m}k} z^{-1} + e^{j\frac{2\pi}{m}k} e^{-j\frac{2\pi}{m}k} z^{-2}} \\ &= \frac{H(k) + H^*(k) - z^{-1} [H(k) e^{-j\frac{2\pi}{m}k} + H^*(k) e^{j\frac{2\pi}{m}k}]}{1 - 2 \cos\left(\frac{2\pi}{m}k\right) z^{-1} + z^{-2}} \end{aligned}$$

When $H(k) + H^*(k)$, we obtain the number
as twice of the real part of $H(k)$. 96

eg- $H(k) = 2 + 3j^0$

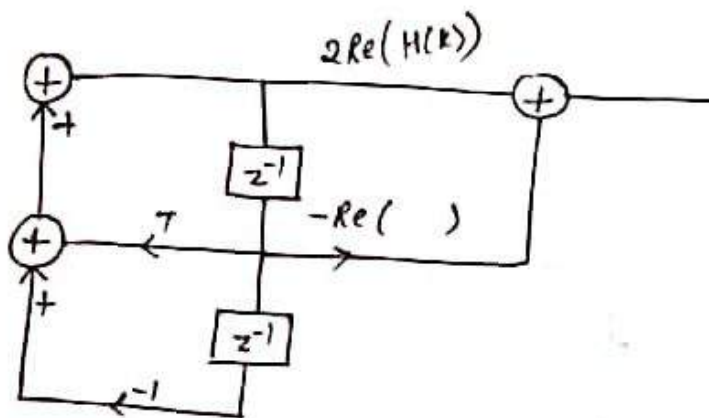
$H^*(k) = 2 - 3j^0$

$\Rightarrow H(k) + H^*(k) = 4 = 2 \operatorname{Re} H(k)$

\therefore

$$H_2(z) = \frac{2 \operatorname{Re}[H(k)] - z^{-1} \left[2 \operatorname{Re}[H(k) \cdot e^{-j \frac{2\pi}{m} k}] \right]}{1 - 2 \cos\left(\frac{2\pi}{m} k\right) \cdot z^{-1} + z^{-2}}$$

$$\frac{1}{1 - 2z^{-1} + z^{-2}}$$



Ques. Let $H(n) = \{1/2, 1, 1/2\}$
Find $H(K)$

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and frequency sampling structure

$$H(K) = \{2, -0.25 - 0.433j, -0.25 + 0.433j\}$$

here, $M = 3$.

$$H(z) = \left[\frac{1-z^{-3}}{3} \right] \cdot \left[\frac{2 \operatorname{Re}(H(1)) - 2 \operatorname{Re}(H(1) e^{-j \frac{2\pi}{3}})}{1 - 2 \cos\left(\frac{2\pi}{3}\right) z^{-1} + z^{-2}} \right] \cdot \frac{H(0)}{1-z^{-1}}$$

$$H(z) = \left[\frac{1-z^{-3}}{3} \right] \cdot \left[\frac{-0.5 - 2 \operatorname{Re} \left[(-0.25 - 0.433j) \cdot e^{-j \frac{2\pi}{3}} \right]}{1 - 2 \cos\left(\frac{2\pi}{3}\right) z^{-1} + z^{-2}} \right] \cdot \frac{H(0)}{1-z^{-1}}$$

$$H(z) = \left[\frac{1-z^{-3}}{3} \right] \cdot \left[\frac{-0.5 - 2 \times 0.5 z^{-1}}{1 - 2 \cos\left(\frac{2\pi}{3}\right) z^{-1} + z^{-2}} \right] \cdot \frac{H(0)}{1-z^{-1}}$$

$$-0.25 + 0.433j$$

$$-2 \cos\left(\frac{2\pi}{3}\right) = -1$$

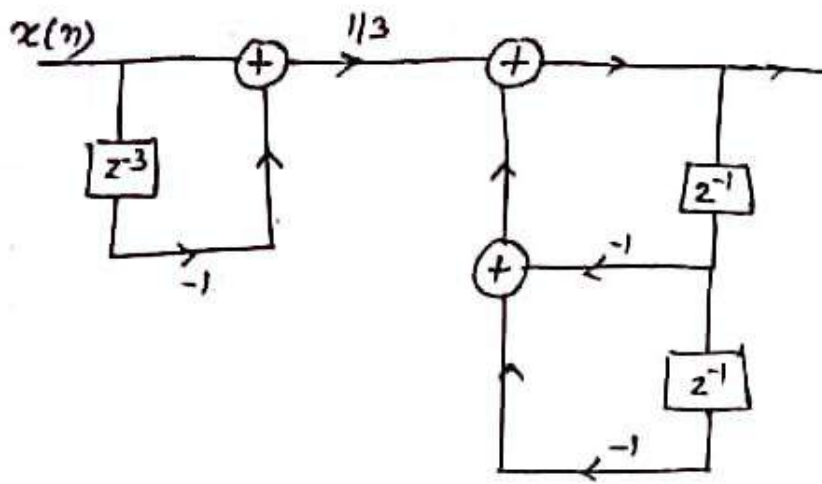
$$e^{-j \frac{2\pi}{3}} =$$

$$\cos \frac{2\pi}{3} - j \sin \frac{2\pi}{3}$$

$$H(z) = \left[\frac{1-z^{-3}}{3} \right] \cdot \left[\frac{-0.5 + 0.5 z^{-1}}{1 + z^{-1} + z^{-2}} \right] + \left[\frac{H(0)}{1-z^{-1}} \right]$$

$$H(0) = 2.$$

$$H(z) = \left[\frac{1-z^{-3}}{3} \right] \cdot \left[\frac{-0.5 + 0.5 z^{-1}}{1 + z^{-1} + z^{-2}} + \frac{2}{1-z^{-1}} \right]$$



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Ques. Conversion of non-recursive structures to Recursive structures -

$$H(z) = \sum_{n=0}^{m-1} h(n) \cdot z^{-n} = \sum_{n=0}^{m-1} b_n \cdot z^{-n}$$

$$b_0 = b_1 = b_2 = b_3 \dots = b_n = b$$

all the coefficients should be same.

\therefore

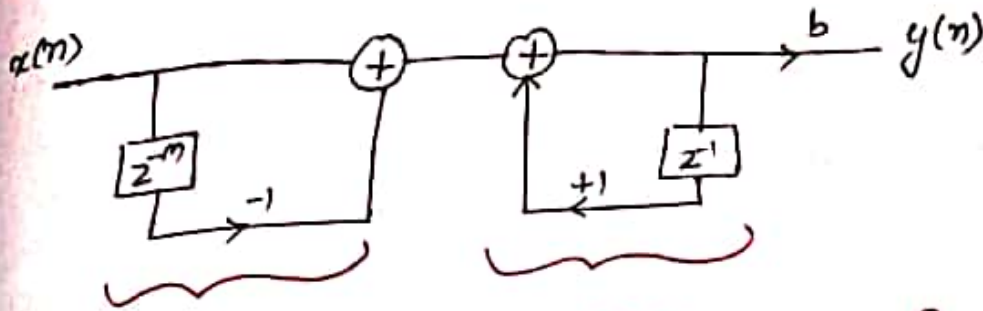
$$H(z) = \sum_{n=0}^{m-1} h(n) \cdot z^{-n} = \sum_{n=0}^{m-1} b \cdot z^{-n}$$

$$= b [1 + z^{-1} + z^{-2} + z^{-3} + \dots + z^{-(m-1)}]$$

$$= b \cdot \left(\frac{1 - z^{-m}}{1 - z^{-1}} \right)$$

$$= (1 - z^{-m}) \cdot \frac{b}{(1 - z^{-1})}$$

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This is called
as comp filter

There's no feedback
here, hence this
is the Non-recursive
part.

This is called Resonators filters.

There are feedback hence,

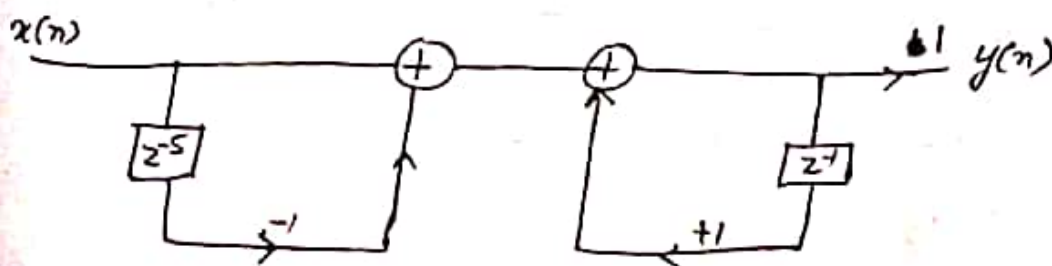
this is the Recursive part.

Ques. Convert the non-recursive structure of-

$$H(z) = 1 + z^{-1} + z^{-2} + z^{-3} + z^{-4}$$

All the coefficients are same hence, it can be converted into the summation of Recursive and non-recursive part.

$$H(z) = \frac{1 - z^{-5}}{1 - z^{-1}}$$



• Poly Phase Structures -

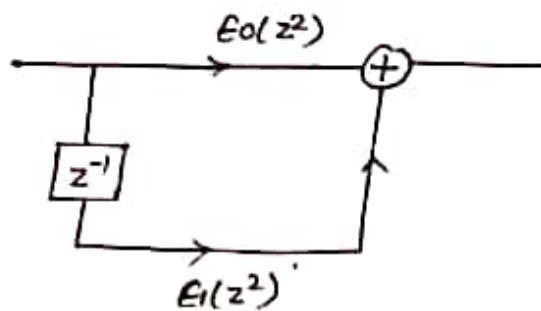
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$$H(z) = \sum_{n=0}^{m-1} h(n) \cdot z^{-n}$$

Dividing $h(n)$ into two parts as even and odd.

$$H(z) = \sum_{n=0}^{\frac{m-1}{2}} h(2n) z^{-2n} + \sum_{n=0}^{\frac{m-1}{2}-1} h(2n+1) z^{-(2n+1)}$$

$$= E_0(z^2) + z^{-1} E_1(z^2)$$



Suppose $m=9$,

$$H(z) = \sum_{n=0}^8 h(n) z^{-n}$$

$$= h(0) + h(1)z^{-1} + h(2)z^{-2} + h(3)z^{-3} + h(4)z^{-4} + h(5)z^{-5} + h(6)z^{-6} + h(7)z^{-7} + h(8)z^{-8}$$

E_0 represents the Even terms;

$$E_0 = h(0) + h(2)z^{-2} + h(4)z^{-4} + h(6)z^{-6} + h(8)z^{-8}$$

E_1 represents the odd terms;

$$E_1 = h(1)z^{-1} + h(3)z^{-3} + h(5)z^{-5} + h(7)z^{-7}$$

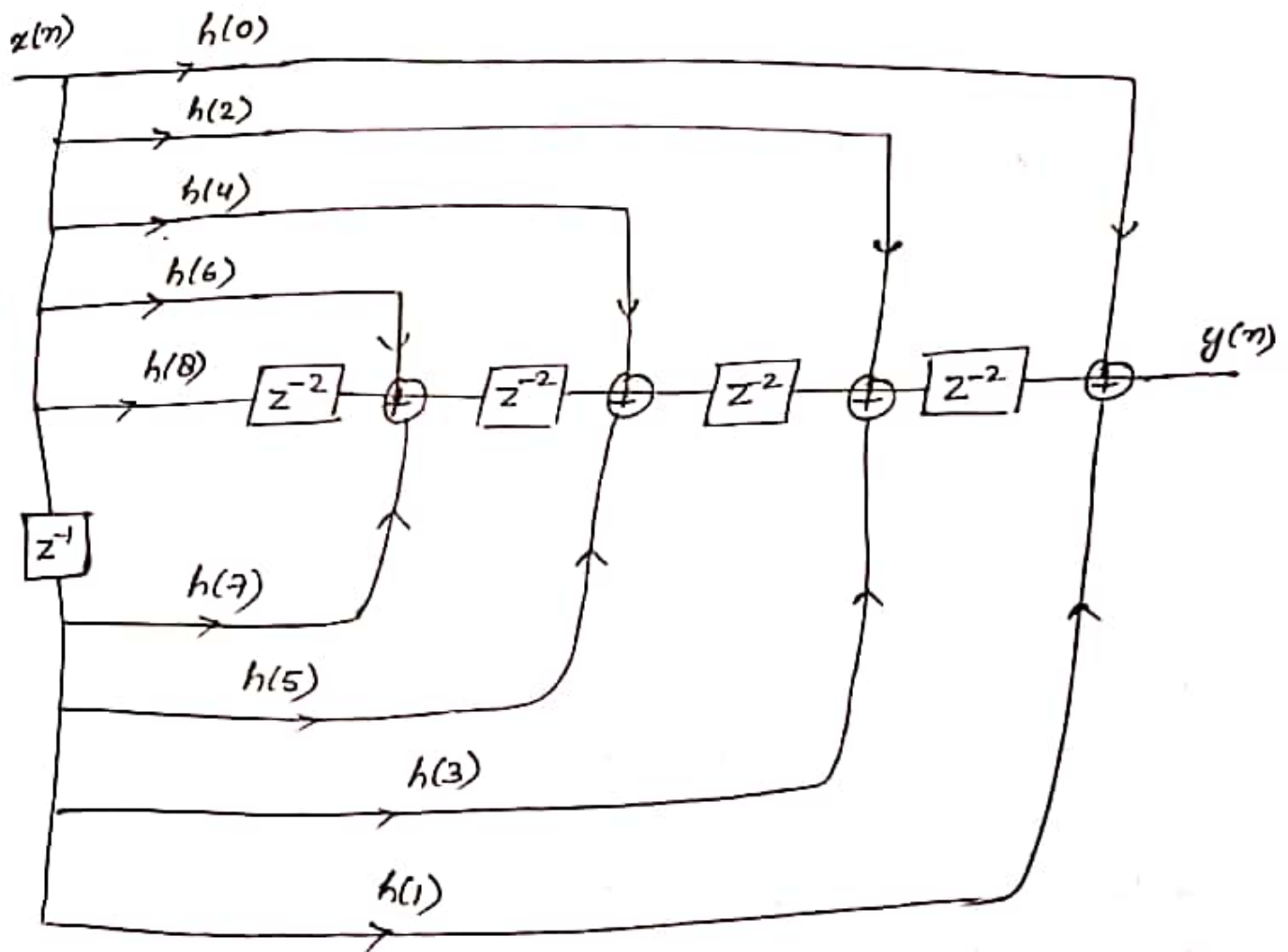
$$E(1) = z^{-1} [h(1) + h(3)z^{-2} + h(5)z^{-4} + h(7)z^{-6}] \quad |01$$

All the powers in $E(0)$ and $E(1)$ are the multiples of 2.

\therefore

$$H(z) = E_0(z^2) + z^{-1} E_1(z^2)$$

$$H(z) = h(0) + h(2)z^{-2} + h(4)z^{-4} + h(6)z^{-6} + h(8)z^{-8} + z^{-1} [h(1) + h(3)z^{-2} + h(5)z^{-4} + h(7)z^{-6}]$$



Applications -

↳ Used in hardware utilization.

↳ Used as multirate process.

$$H(z) = \frac{\sum_{k=0}^{m-1} b_k \cdot z^{-k}}{1 + \sum_{k=1}^{N-1} a_k \cdot z^{-k}} \quad \text{--- (1)}$$

There are two forms in this -

↳ Direct I form

(we consider zeroes first and then the poles)

↳ Direct II form.

(we consider poles first and then the zeroes.)

• Direct-I form -

$$H(z) = \frac{Y(z)}{X(z)} = \underbrace{\frac{W(z)}{X(z)}}_{\text{Zeroes}} \cdot \underbrace{\frac{Y(z)}{W(z)}}_{\text{Poles}}$$

$$\frac{W(z)}{X(z)} = \sum_{k=0}^{m-1} b_k \cdot z^{-k} \quad \{ \text{from eq}^n (1) \}$$

suppose, $m = 4$

$$= \sum_{k=0}^3 b_k \cdot z^{-k}$$

$$\frac{w(z)}{x(z)} = b_0 + b_1 z^{-1} + b_2 z^{-2} + b_3 z^{-3}$$

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$$\Rightarrow w(z) = [b_0 + b_1 z^{-1} + b_2 z^{-2} + b_3 z^{-3}] \cdot x(z)$$

Taking its inverse;

$$w(n) = b_0 x(n) + b_1 x(n-1) + b_2 x(n-2) + b_3 x(n-3) \quad \text{---(2)}$$

$$\frac{y(z)}{w(z)} = \frac{1}{1 + \sum_{k=1}^{N-1} a_k z^{-k}} \quad \left\{ \text{from eqn (1)} \right\}$$

suppose, $N=4$

$$\Rightarrow y(z) \cdot \left[1 + \sum_{k=1}^3 a_k z^{-k} \right] = w(z)$$

$$\Rightarrow y(z) \cdot [1 + a_1 z^{-1} + a_2 z^{-2} + a_3 z^{-3}] = w(z)$$

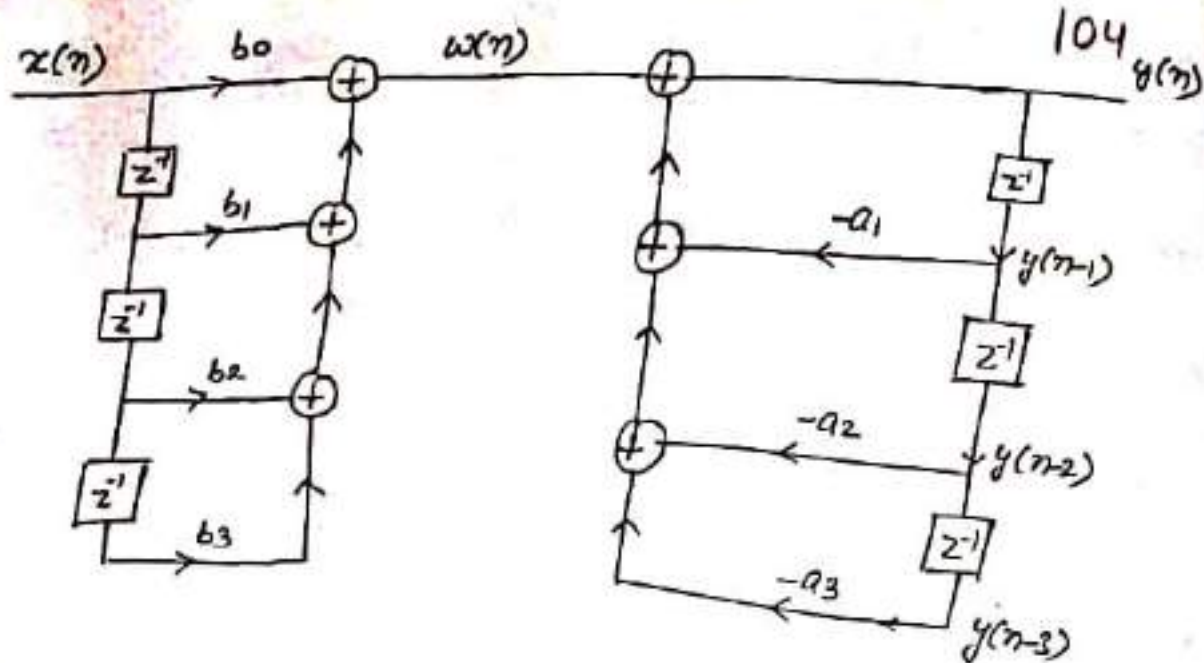
$$\Rightarrow y(z) + a_1 z^{-1} y(z) + a_2 z^{-2} y(z) + a_3 z^{-3} y(z) = w(z)$$

Taking its inverse;

$$w(n) = y(n) + a_1 y(n-1) + a_2 y(n-2) + a_3 y(n-3)$$

$$\Rightarrow y(n) = w(n) - a_1 y(n-1) - a_2 y(n-2) - a_3 y(n-3) \quad \text{---(3)}$$

IR systems are always Recursive i.e., they always have a feedback.



Q No. of multipliers used in this will be = $m+n-1$

No. of delays used in this will be = $m+n-2$

No. of adders used in this will be = $m+n-2$

6th April, 19

$$H(z) = H_1(z) \cdot H_2(z)$$

$$= \frac{\omega(z)}{X(z)} \cdot \frac{Y(z)}{\omega(z)}$$

$\underbrace{X(z)}_{\text{pole}} \quad \underbrace{\omega(z)}_{\text{zero}}$

$$= \frac{\sum_{k=0}^{m-1} b_k \cdot z^{-k}}{1 + \sum_{k=1}^{m-1} a_k \cdot z^{-k}} \quad (M=4)$$

for pole,

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$$\frac{W(z)}{X(z)} = \frac{1}{1 + a_1 z^{-1} + a_2 z^{-2} + a_3 z^{-3}}$$

$$W(z) + a_1 z^{-1} W(z) + a_2 z^{-2} W(z) + a_3 z^{-3} W(z) = X(z)$$

$$W(n) + a_1 W(n-1) + a_2 W(n-2) + a_3 W(n-3) = X(n)$$

(from time shifting property)

$$W(n) = X(n) - a_1 W(n-1) - a_2 W(n-2) - a_3 W(n-3)$$

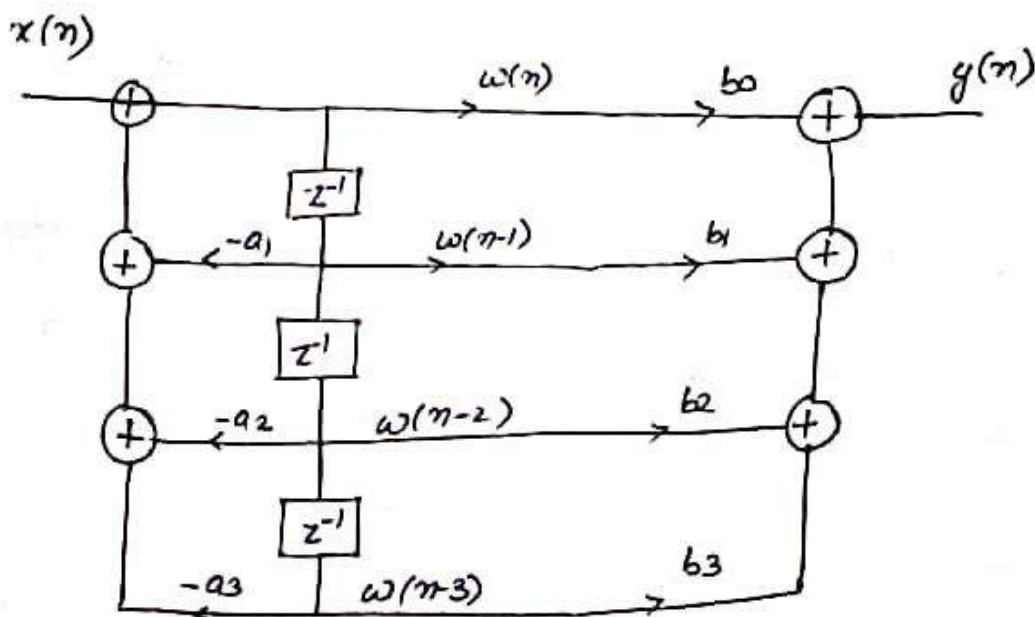
for zero,

(1)

$$\frac{Y(z)}{W(z)} = \sum_{k=0}^{m-1} w_k z^{-k} \quad (M=4)$$

$$= b_0 + b_1 z^{-1} + b_2 z^{-2} + b_3 z^{-3}$$

$$y(n) = b_0 W(n) + b_1 W(n-1) + b_2 W(n-2) + b_3 W(n-3)$$



No. of multipliers = 7

No. of delays = max. of $m-1$

Ques: Obtain Direct-I form and Direct-II form
Imp: for $H(z) = \frac{1 + 2z^{-1} - z^{-2}}{1 + z^{-1} - z^{-2}}$ 106

• Direct-II form-

$$H(z) = \frac{1 + 2z^{-1} - z^{-2}}{1 + z^{-1} - z^{-2}} = \underbrace{\frac{w(z)}{x(z)}}_{\text{for pole}} \cdot \underbrace{\frac{y(z)}{w(z)}}_{\text{for zero}}$$

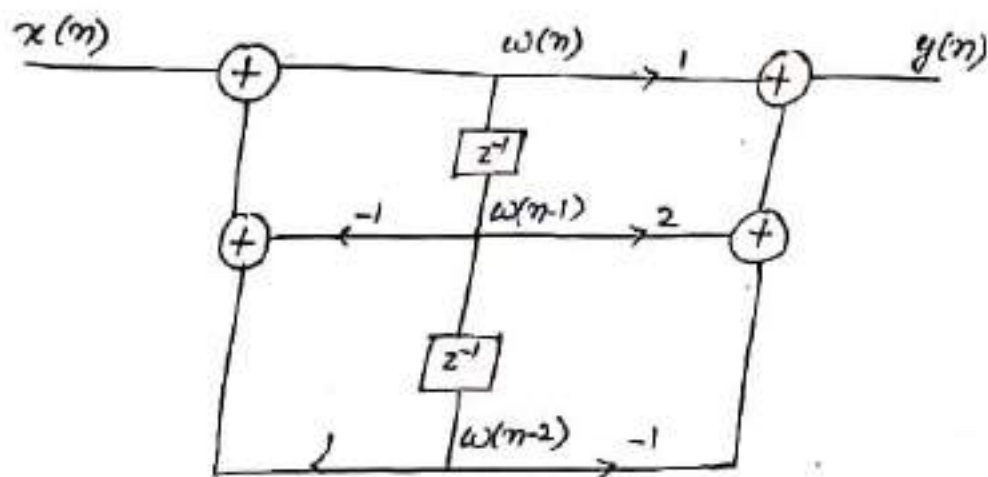
$$\frac{w(z)}{x(z)} = \frac{1}{1 + z^{-1} - z^{-2}}$$

$$\frac{y(z)}{w(z)} = 1 + 2z^{-1} - z^{-2}$$

$$w(n) = x(n) - w(n-1) + w(n-2)$$

and,

$$y(n) = w(n) + 2w(n-1) - w(n-2)$$



• Direct I form -

(Reverse of direct-II form)

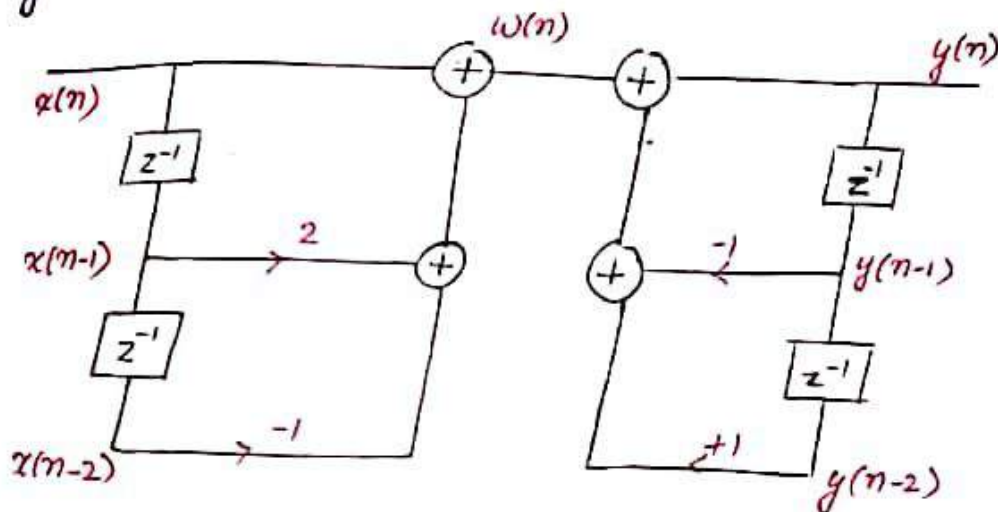
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$$\frac{W(z)}{X(z)} = 1 + 2z^{-1} - z^{-2}$$

$$\frac{Y(z)}{W(z)} = \frac{1}{1 + z^{-1} - z^{-2}}$$

$$W(n) = x(n) + 2x(n-1) - x(n-2)$$

$$y(n) = W(n) - y(n-1) + y(n-2)$$



multiplexer = 5

delay = 4

• Cascade Form -

$$H(z) = \frac{b_0 + b_1 z^{-1} + b_2 z^{-2} + \dots + b_{m-1} z^{-(m-1)}}{1 + a_1 z^{-1} + a_2 z^{-2} + \dots + a_{N-1} z^{-(N-1)}}$$

$$b_0 \prod_{k=1}^{\frac{N-1}{2}} \frac{(1 + B_{1k} z^{-1} + B_{2k} z^{-2})}{(1 + A_{1k} z^{-1} + A_{2k} z^{-2})} ; N \text{ is odd}$$

$$= b_0 \frac{(1 + b_{10} z^{-1})}{(1 + a_{10} z^{-1})} \prod_{k=1}^{\frac{N-2}{2}} \left(\frac{1 + B_{1k} z^{-1} + B_{2k} z^{-2}}{1 + A_{1k} z^{-1} + A_{2k} z^{-2}} \right) ; N \text{ is even}$$

Ques. Obtain the cascade structure of -

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$$H(z) = \frac{1 + \frac{1}{4}z^{-1} + \frac{1}{2}z^{-2}}{(1 + \frac{1}{2}z^{-1})(1 + z^{-1} + \frac{1}{2}z^{-2})(1 + \frac{1}{2}z^{-1} + \frac{1}{4}z^{-2})}$$

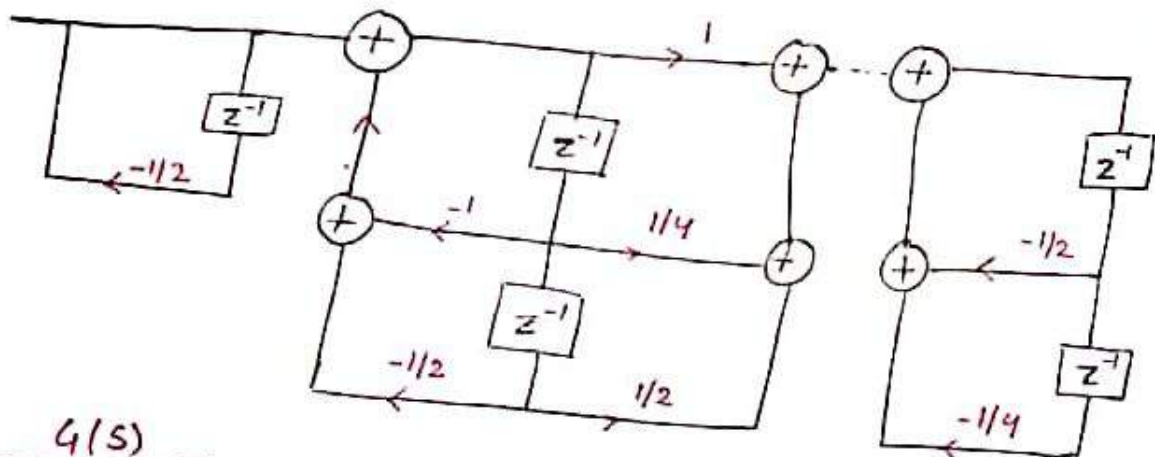
$$(1 + \frac{1}{2}z^{-1})(1 + z^{-1} + \frac{1}{2}z^{-2})(1 + \frac{1}{2}z^{-1} + \frac{1}{4}z^{-2})$$

No even = 6

$$b_0 = 1$$

$$b_{10} = 0$$

$$H(z) = \frac{1}{(1 + \frac{1}{2}z^{-1})} \cdot \frac{(1 + \frac{1}{4}z^{-1} + \frac{1}{2}z^{-2})}{(1 + z^{-1} + \frac{1}{2}z^{-2})} \cdot \frac{1}{(1 + \frac{1}{2}z^{-1} + \frac{1}{4}z^{-2})}$$



$$\frac{G(s)}{1 + G(s) \cdot H(s)}$$

$$G(s) = 1$$

$$H(s) = \frac{1}{2}z^{-1}$$

• Parallel Form Structure :-

$$H(z) = \frac{b_0 + b_1z^{-1} + b_2z^{-2} + \dots + b_{m-1}z^{-(m-1)}}{1 + a_1z^{-1} + a_2z^{-2} + \dots + a_{N-1}z^{-(N-1)}}$$

When, $m < N$

where m is the maximum power in the numerator

N is the maximum power in the denominator.

$$H(z) = \begin{cases} \sum_{k=1}^{\frac{N-1}{2}} \frac{B_{0k} + B_{1k}z^{-1}}{1 + A_{1k}z^{-1} + A_{2k}z^{-2}} & ; N \text{ is odd. } 109 \\ \frac{b_{10}}{1 + a_{10}z^{-1}} + \sum_{k=1}^{\frac{N-2}{2}} \frac{B_{0k} + B_{1k}z^{-1}}{1 + A_{1k}z^{-1} + A_{2k}z^{-2}} & ; N \text{ is even} \end{cases}$$

When $m > N$,

$$H(z) = \begin{cases} \sum_{k=0}^{m-N} c_k z^{-k} + \sum_{k=1}^{\frac{N-1}{2}} \frac{B_{0k} + B_{1k}z^{-1}}{1 + A_{1k}z^{-1} + A_{2k}z^{-2}} & ; N \text{ is odd} \\ \sum_{k=0}^{m-N} c_k z^{-k} + \frac{b_{10}}{1 + a_{10}z^{-1}} + \sum_{k=1}^{\frac{N-2}{2}} \frac{B_{0k} + B_{1k}z^{-1}}{1 + A_{1k}z^{-1} + A_{2k}z^{-2}} & ; N \text{ is even} \end{cases}$$

When $m = N$,

there will be a constant term or value i.e. c_k .

Ques. $H(z) = \frac{1 + \frac{1}{4}z^{-1}}{(1 + \frac{1}{2}z^{-1})(1 + \frac{1}{2}z^{-1} + \frac{1}{4}z^{-2})}$ $m=2$
 $N=4$

$$H(z) = \frac{b_{10}}{1 + a_{10}z^{-1}} + \sum_{k=1}^{\frac{N-2}{2}} \frac{B_{0k} + B_{1k}z^{-1}}{1 + A_{1k}z^{-1} + A_{2k}z^{-2}}$$

$$= \frac{b_{10}}{1 + a_{10}z^{-1}} + \frac{B_{01} + B_{11}z^{-1}}{1 + A_{11}z^{-1} + A_{21}z^{-2}}$$

$$= \frac{b_{10} [1 + A_{11}z^{-1} + A_{21}z^{-2}] + [B_{01} + B_{11}z^{-1}] \cdot [1 + a_{10}z^{-1}]}{(1 + a_{10}z^{-1}) \cdot (1 + A_{11}z^{-1} + A_{21}z^{-2})}$$

$$= \frac{b_{10} + b_{10}A_{11}z^{-1} + b_{10}A_{21}z^{-2} + B_{01} + B_{11}z^{-1} + B_{10}a_{10}z^{-1} + B_{11}a_{10}z^{-2}}{(1 + a_{10}z^{-1}) \cdot (1 + A_{11}z^{-1} + A_{21}z^{-2})}$$

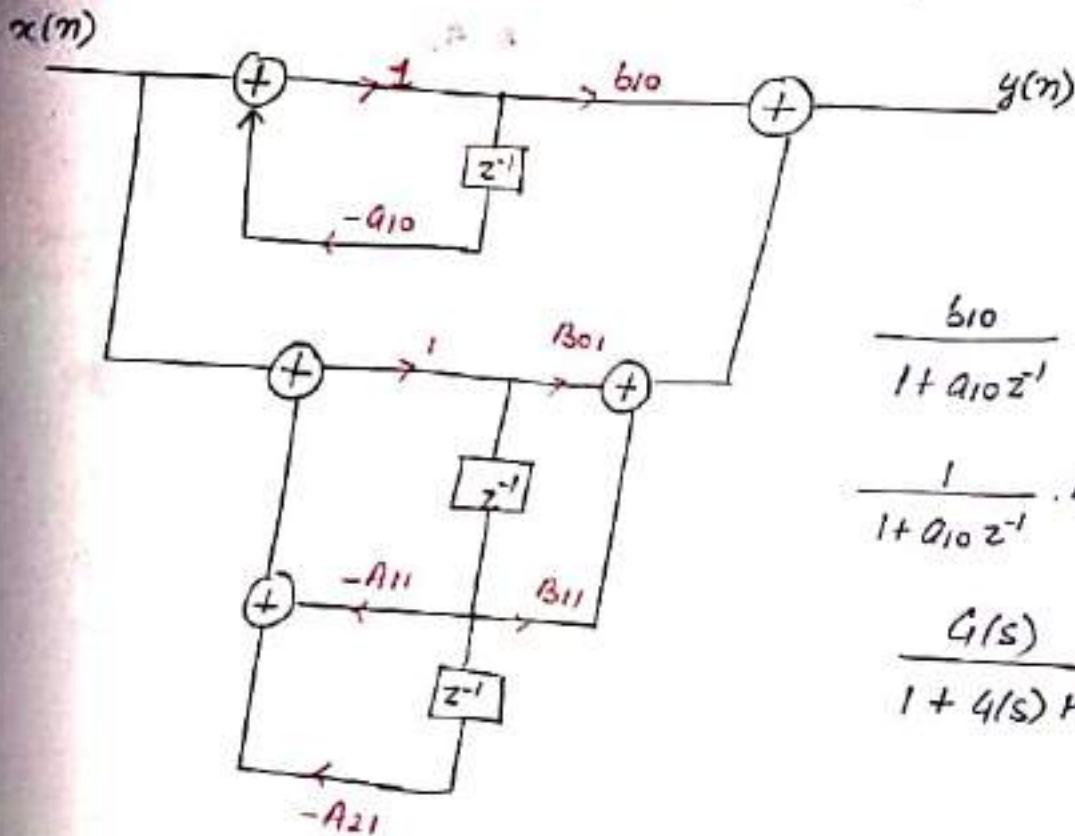
$$A_{11} = 1/2$$

$$a_{11} = 1/2$$

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$$A_{21} = 1/4$$

$$= \frac{b_{10} + b_{10} \frac{1}{2} z^{-1} + b_{10} \cdot \frac{1}{4} z^{-2} + B_{01} \cdot (1) + B_{10} \cdot \frac{1}{2} z^{-1} + B_{11} z^{-1} + B_{11} \frac{1}{2} z^{-2}}{(1 + \frac{1}{2} z^{-1}) \cdot (1 + \frac{1}{2} z^{-1} + \frac{1}{4} z^{-2})}$$



$$\frac{b_{10}}{1 + a_{10} z^{-1}}$$

$$\frac{1}{1 + a_{10} z^{-1}} \cdot b_{10}$$

$$\frac{G(s)}{1 + G(s) H(s)} \cdot b_{10}$$

Polyphase Structure :-

$$H(z) = \underbrace{E_0(z^2)}_{\downarrow} + z^{-1} \underbrace{E_1(z^2)}_{\downarrow}$$

represents the
even part of
 $x(z)$

represents the odd
part of $x(z)$.

Ques. Obtain the polyphase structure of -

$$H(z) = \frac{1-2z^{-1}}{1+3z^{-1}}$$

$$x(t) = x_e + x_o$$

$$x_e = \frac{x(t) + x(-t)}{2}$$

$$x_o = \frac{x(t) - x(-t)}{2}$$

$$\therefore E_0(z^2) = \frac{H(z) + H(-z)}{2} = \frac{\frac{1-2z^{-1}}{1+3z^{-1}} + \frac{1+2z^{-1}}{1-3z^{-1}}}{2}$$

$$= \frac{(1-2z^{-1})(1-3z^{-1}) + (1+3z^{-1})(1+2z^{-1})}{2 \cdot (1+3z^{-1})(1-3z^{-1})}$$

$$= \frac{1-3z^{-1}-2z^{-1}+6z^{-1} + 1+2z^{-1}+3z^{-1}+6z^{-1}}{2 \cdot [(1)^2 - (3z^{-1})^2]}$$

$$= \frac{2+12z^{-2}}{2[1-9z^{-2}]} = \frac{1+6z^{-2}}{1-9z^{-2}}$$

$$z^{-1} E_1(z^2) = \frac{H(z) - H(-z)}{2}$$

$$= \frac{1-2z^{-1}}{1+3z^{-1}} - \frac{1+2z^{-1}}{1-3z^{-1}}$$

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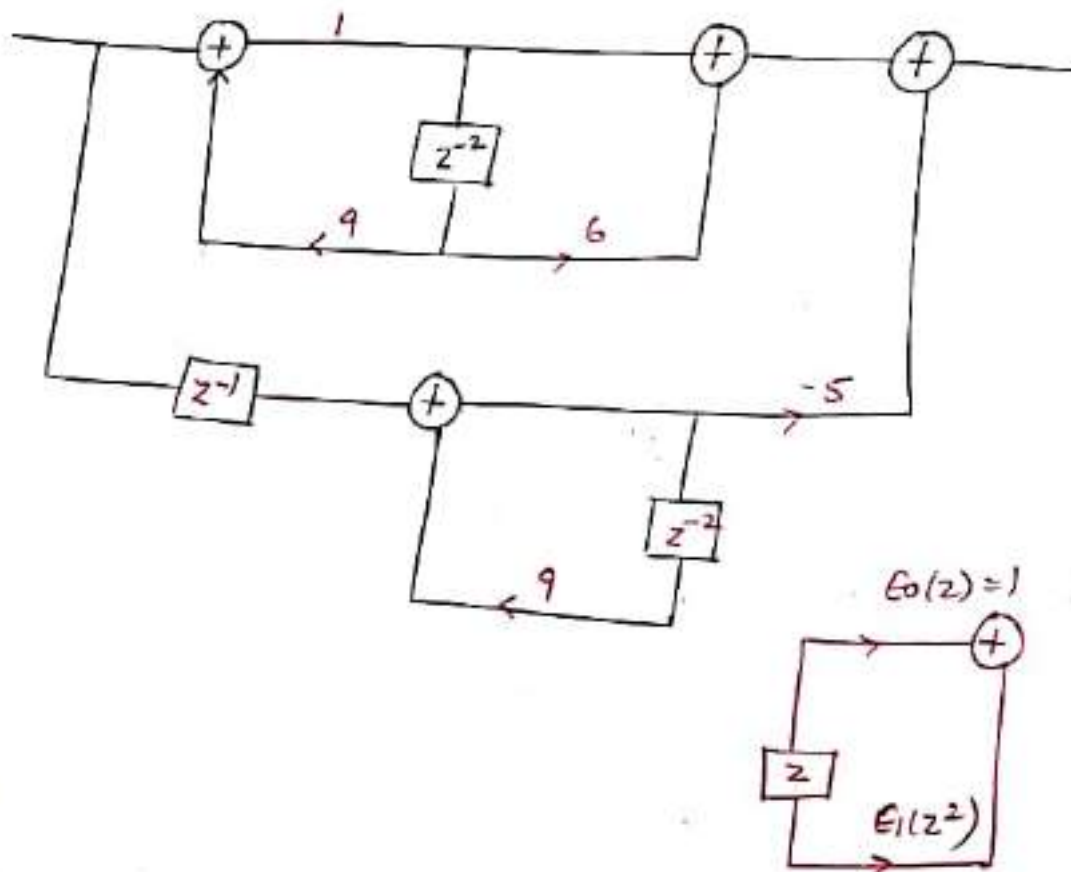
$$= \frac{(1-2z^{-1})(1-3z^{-1}) - (1+2z^{-1})(1+3z^{-1})}{2[(1)^2 - (3z^{-1})^2]}$$

$$= \frac{1-3z^{-1}-2z^{-1}+6z^{-2}-1-2z^{-1}-3z^{-1}-6z^{-2}}{2[1-9z^{-2}]}$$

$$z^{-1} E_1(z^2) = \frac{-5z^{-1}}{1-9z^{-2}}$$

$$\therefore H(z) = E_0(z^2) + z^{-1} E_1(z^2)$$

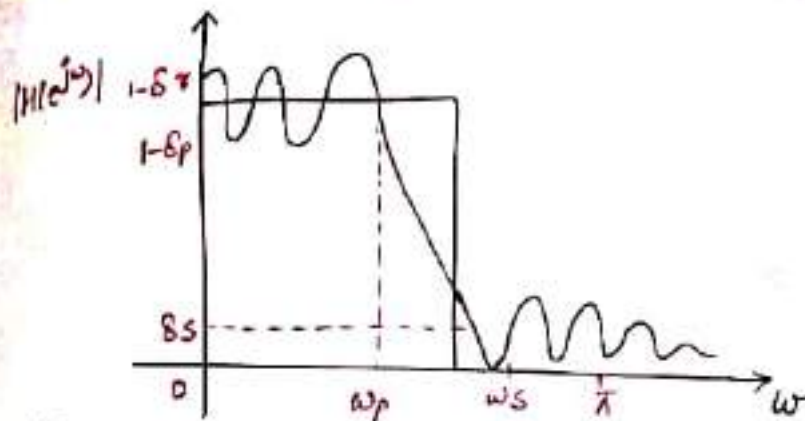
$$= \frac{1+6z^{-2}}{1-9z^{-2}} + \left(\frac{-5z^{-1}}{1-9z^{-2}} \right)$$



Fir Specifications -

(A) Absolute Specification -

(for FIR)

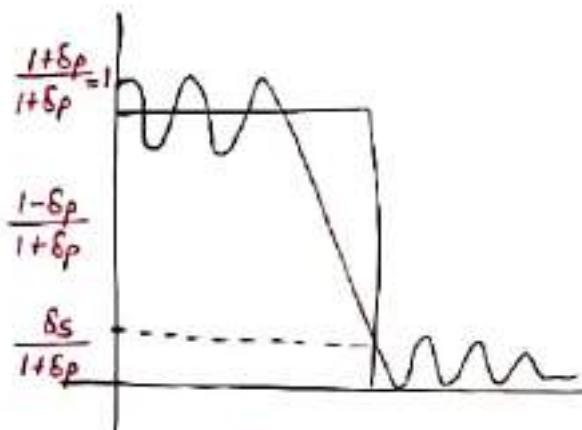

 δ_p
 δ_s

$$\Delta\omega = \omega_s - \omega_p$$

$$1 - \delta_p \leq |H(e^{j\omega})| \leq 1 + \delta_p \quad 0 \leq \omega \leq \omega_p$$

$$|H(e^{j\omega})| \leq \delta_s \quad \omega_s \leq \omega \leq \pi$$

(B) Relative Specification -

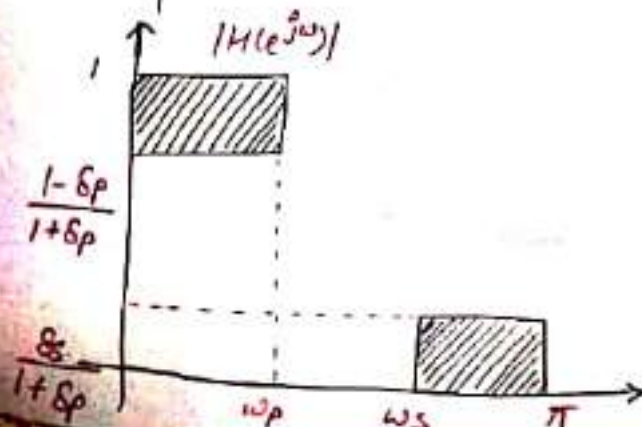


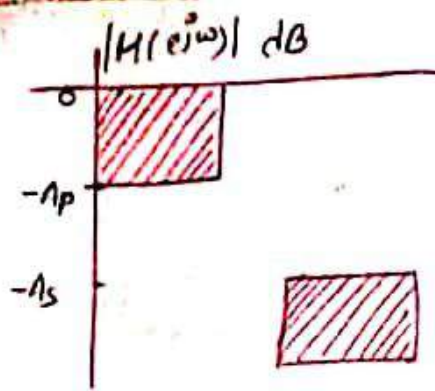
$$\frac{1 - \delta_p}{1 + \delta_p} \leq |H(e^{j\omega})| \leq 1$$

$$0 \leq \omega \leq \omega_p$$

$$|H(e^{j\omega})| \leq \frac{\delta_s}{1 + \delta_p}$$

$$\omega_s \leq \omega \leq \pi$$





$$A_p = 20 \log \left(\frac{1 + \delta_p}{1 - \delta_p} \right)$$

$$A_s = 20 \log \left(\frac{1 + \delta_p}{\delta_s} \right) \quad \text{or} \quad -20 \log \delta_s$$

$$\delta_p = \frac{10^{A_p/20} - 1}{10^{A_p/20} + 1}$$

and,

$$\delta_s = 10^{-A_s/20}$$

Analog Filter Specification- (for IR)

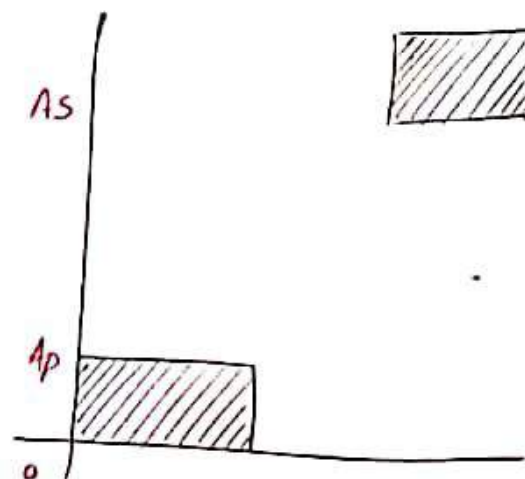
- * Attenuation in pass band is minimum.
- * Attenuation in stop band is maximum.

$\delta \rightarrow$ Pass band ripple factor

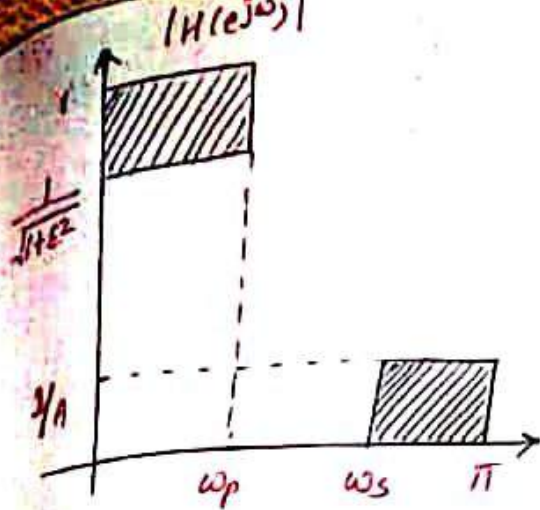
$\delta_s \rightarrow$ Stop band

$\delta_p \rightarrow$ Pass band tolerance

$A \rightarrow$ Stop band ripple factor



Analog filter specifications



$$\delta_1 = \frac{1 - \delta_p}{1 + \delta_p} = \frac{1}{\sqrt{1 + \epsilon^2}} = \epsilon = \sqrt{\frac{1}{\delta_1^2} - 1}$$

$$\frac{1}{A} = \frac{\delta_s}{1 + \delta_p} \quad \Rightarrow \quad \delta_2$$

$$A_p = 20 \log(\sqrt{1 + \epsilon^2})$$

$$A_s = 20 \log(A)$$

$$\epsilon = \sqrt{10^{A_p/10} - 1}$$

$$A = 10^{A_s/20}$$

$$\left\{ \begin{array}{l} \delta_1 = \frac{1 - \delta_p}{1 + \delta_p} \\ \delta_2 = \frac{\delta_s}{1 + \delta_p} \end{array} \right.$$

• FIR Filter Designing -

(1) Windowing Method -

Infinite sequence are converted into finite sequence.

(a) Rectangular windowing method -

Signal is multiplied by the rectangular window. It increases oscillations and ripples in pass and stop band. It is called Gibbs effect.

$H_d(n)$ is the input of infinite range.

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$$H_d(n) \cdot \omega(n)$$

$$H_m(n) = H_d(n) \cdot \omega(n)$$

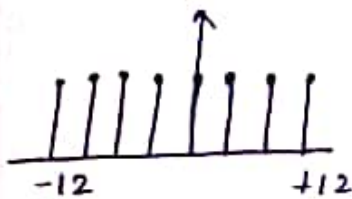
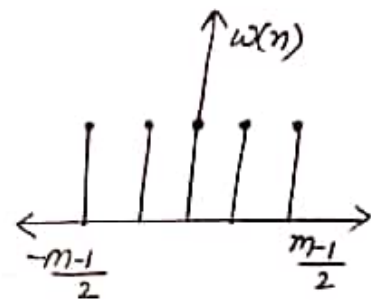
range is finite

In terms of frequency,

$$H_m(e^{j\omega}) = H_d(e^{j\omega}) \otimes \omega(e^{j\omega}) \quad \text{periodic convolution}$$

$$= \frac{1}{2\pi} \int H_d(e^{j\omega}) \cdot \omega(e^{j\omega-\theta}) d\theta$$

Assume the length of the filter is 25.

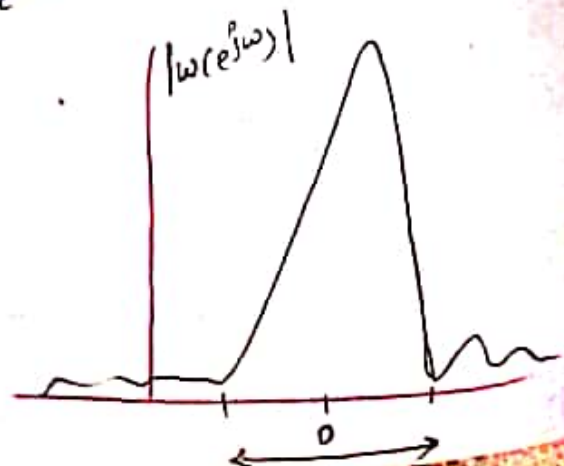


$$\omega(e^{j\omega}) = \sum_{n=-\frac{m-1}{2}}^{\frac{m-1}{2}} 1 \cdot e^{-j\omega n}$$

$$\Rightarrow k = n + \left(\frac{m-1}{2}\right)$$

$$\begin{aligned} \therefore \omega(e^{j\omega}) &= \sum_{k=0}^{m-1} e^{-j\omega \left[k - \frac{m-1}{2}\right]} \\ &= e^{+j\omega \left(\frac{m-1}{2}\right)} \sum_{k=0}^{m-1} e^{-j\omega k} \end{aligned}$$

$$\omega(e^{j\omega})^* = \frac{\sin \frac{\omega m}{2}}{\sin \frac{\omega}{2}}$$



To find the transition width -

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$$\sin \frac{\omega m}{2} = 0 = \sin n\pi$$

$$m = \pm 1, \pm 2, \pm 3, \dots$$

$$m = 1$$

$$\frac{\omega m}{2} = n\pi$$

$$\boxed{\omega = \frac{2\pi}{m}}$$

Transition width, $D = 2\omega = \frac{4\pi}{m}$, where m is the length of the filter.

$$\sin \frac{\omega m}{2} = 1 = \sin \frac{n\pi}{2}$$

$$m = \pm 3, \pm 5, \pm 7, \dots$$

For $n = 3$,

$$\frac{\omega m}{2} = \frac{3\pi}{2}$$

$$\boxed{\omega = \frac{3\pi}{m}} ; \text{ for maximum side lobe}$$

$$\left| \omega(e^{j\omega}) \right|_{\omega = \frac{3\pi}{m}} = \frac{\sin \frac{3\pi}{m} \frac{m}{2}}{\sin \frac{3\pi}{m_2}} = \frac{\sin \frac{3\pi}{2}}{\sin \frac{3\pi}{m_2}}$$

where, m is large.

$$= \frac{1}{(3\pi/m_2)}$$

$$\boxed{\left| \omega(e^{j\omega}) \right|_{\omega = \frac{3\pi}{m}} = \frac{2m}{3\pi}}$$

Magnitude of first side lobe.

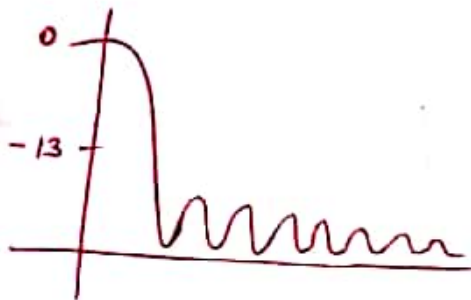
Magnitude of the main lobe = m .

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Decrement in lobe in respect to the main lobe

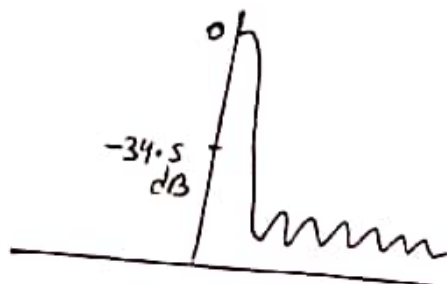
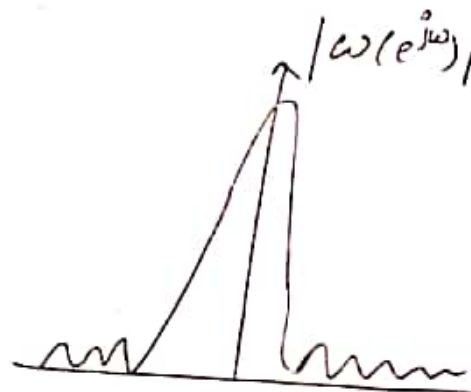
$$= \frac{\text{side lobe}}{\text{main lobe}} \times 100$$

$$= \frac{\left(\frac{2m}{3\pi}\right)}{m} \times 100 = \frac{2}{3\pi} \times 100 = -13 \text{ dB}$$



On increasing the values, fluctuations will be lesser.

(b) Kaiser Window-



$$w(n) = \begin{cases} \frac{I_0 \left[\beta \sqrt{1 - \left(1 - \frac{2n}{m-1}\right)^2} \right]}{I_0(\beta)} & ; 0 \leq n \leq m-1 \text{ (for causal)} \\ 0 & ; \text{otherwise} \end{cases}$$

$$D(n) = \begin{cases} \frac{T_0 \left[\beta \sqrt{1 - \left(\frac{2m}{m-1} \right)^2} \right]}{T_0(\beta)} & -\frac{m-1}{2} \leq n \leq \frac{m-1}{2} \end{cases} \quad 119$$

$$T_0(\beta) = 1 + \sum_{\beta=1}^{\infty} \left[\frac{1}{\beta!} \left(\frac{\pi}{2} \right)^{\beta} \right]^2$$

filter designing using Kaiser Window -

(i) Find δ_p and δ_s .

$$\delta_p = \frac{10^{A_p/20} - 1}{10^{A_p/20} + 1} \quad \text{and} \quad \delta_s = 10^{-A_s/20}$$

$$\delta = \min(\delta_p, \delta_s)$$

here in, δ_s is always less.

(2) Find attenuation

$$A = -20 \log_{10} \delta$$

(3) Find transition width.

$$\Delta\omega = \omega_s - \omega_p$$

$$\Delta f = \frac{\omega_s - \omega_p}{2\pi}$$

(4) Find m .

$$m \geq \begin{cases} \frac{A - 7.95}{14.36 \Delta f} + 1 & A \geq 21 \text{ dB} \\ \frac{0.922}{\Delta f} + 1 & A < 21 \text{ dB} \end{cases}$$

(5) To find β

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$$\beta = \begin{cases} 0 & A \leq 21 \\ 0.5842(A-21)^{0.4} + 0.07866(A-21) & 21 < A \leq 50 \\ 0.1102(A-8.7) & A > 50 \end{cases}$$

(6) Compute $\omega(n)$

(7) Determine the desired impulse response $H_d(n)$ using inverse DFT.

(8) $H_m(n) = H_d(n) \cdot \omega(n)$

$$h(n) = h(m-1-n)$$

9th April, 19

Ques. Design a low pass filter, with the following specifications - $0.99 < |H(e^{j\omega})| < 1.01$

and the magnitude of

$$|\omega| \leq 0.4\pi$$

$$|H(e^{j\omega})| \leq 0.01$$

$$0.6\pi < |\omega| \leq \pi$$

Using Kaiser window.

Soln. $1 - \delta_p = 0.99$

$$1 + \delta_p = 1.01$$

$$\delta_p = 1 - 0.99$$

$$\delta_p = 1.01 - 1$$

$$= 0.01$$

$$= 0.01$$

$$\boxed{\delta_p = 0.01}$$

$$|H(e^{j\omega})| \leq \delta_s$$

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$$\therefore \boxed{\delta_s = 0.01}$$

$$\text{from } 0 \leq |\omega| \leq 0.4\pi$$

$$\omega_p = 0.4\pi$$

$$\text{from } 0.6\pi \leq |\omega| < \pi$$

$$\omega_s = 0.6\pi$$

$$\delta = \min(\delta_p, \delta_s)$$

$$\boxed{\delta = 0.01}$$

$$A = -20 \log(0.01) = 40 \text{ dB}$$

$$\Delta\omega = \omega_s - \omega_p$$

$$\boxed{\Delta\omega = 0.2\pi}$$

$$\Delta f = \frac{\omega_s - \omega_p}{2\pi} = \frac{0.2\pi}{2\pi} = 0.1$$

$$m \geq \frac{A - 7.95}{14.36 \Delta f} + 1 = \frac{40 - 7.95}{14.36 \times 0.1} + 1$$

$$= \frac{32.05}{1.436} + 1 = 23.3189$$

$$\boxed{m = 25}$$

For causal, we can take odd and even both but for anti-causal only odd will be taken.

Generally, causal is taken.

$$\beta = 0.5842 (40-21)^{0.4} + 0.07866 (40-21) \quad 122$$

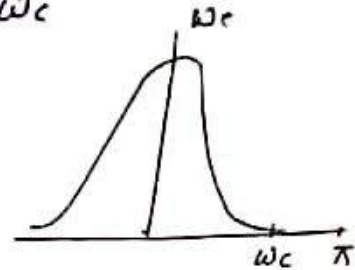
$$25 < A \leq 50$$

$$= 0.5842 (19)^{0.4} + 0.07866 (19)$$

$$= 3.3953$$

$$\omega(n) = \frac{J_0 \left(\beta \sqrt{1 - \left(1 - \frac{2n}{m-1}\right)^2} \right)}{J_0(\beta)} \quad 0 \leq n \leq m-1$$

$$H_m |e^{j\omega}| = \begin{cases} e^{-j\tau\omega} & ; \text{ when } \omega \leq \omega_c \\ 0 & ; \text{ otherwise} \end{cases}$$



$$\tau = \frac{m-1}{2}$$

By symmetry property, we will calculate from 0 to 12.

$$h(0) = h(m-1-n)$$

$$h(0) = h(m-1-0)$$

$$h(0) = h(24)$$

$$h(1) = h(23)$$

$$h_m(n) = \frac{1}{2\pi} \int_{-\omega_c}^{+\omega_c} e^{-j\omega\tau} \cdot e^{j\omega n} \cdot d\omega$$

$$= \frac{1}{2\pi} \int_{-\omega_c}^{+\omega_c} e^{j\omega(-\tau+n)} \cdot d\omega$$

$$= \frac{\sin 0.5\pi(n-12)}{\pi(n-12)}$$

$$\omega_c = \frac{1}{2} (\omega_p + \omega_s)$$

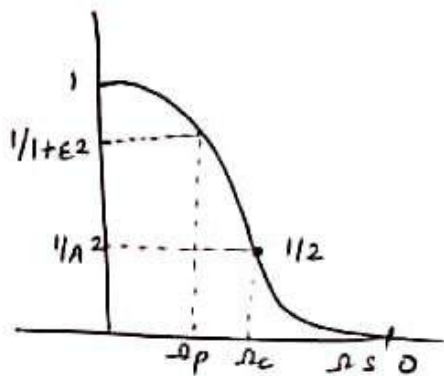
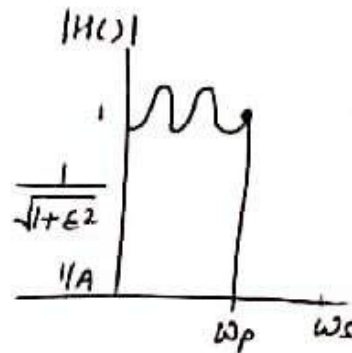
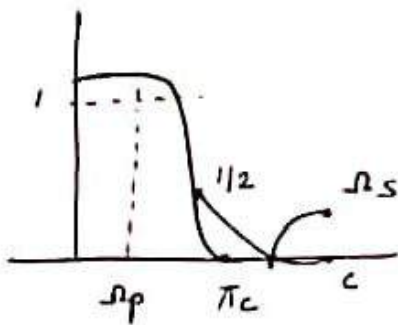
$$= \frac{1}{2} (0.4\pi + 0.6\pi)$$

$$= 0.5\pi$$

Analog Butterworth Filter (IR filter) - 123

$$|H(j\Omega)|^2 = \frac{1}{1 + \left(\frac{\Omega}{\Omega_c}\right)^{2N}}$$

zero oscillations



Ques1 Determination of filter parameters -

(a) N

(b) cut-off frequency, ω_c .

Case I : When specifications ϵ , A , ω_p , ω_s are given

At Ω_p ,

$$|H(j\Omega_p)|^2 = \frac{1}{1 + \left(\frac{\Omega_p}{\Omega_c}\right)^{2N}} = \frac{1}{1 + \epsilon^2}$$

Similarly at Ω_s ,

$$|H(e^{j\Omega_s})|^2 = \frac{1}{1 + \left(\frac{\Omega_s}{\Omega_c}\right)^{2N}} = \frac{1}{A^2} \quad (\text{from graph})$$

$$\epsilon^2 = \left(\frac{\Omega_p}{\Omega_c} \right)^{2N}$$

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$$A^2 - 1 = \left(\frac{\Omega_s}{\Omega_c} \right)^{2N}$$

$$\therefore \frac{\epsilon^2}{A^2 - 1} = \frac{\left(\frac{\Omega_p}{\Omega_c} \right)^{2N}}{\left(\frac{\Omega_s}{\Omega_c} \right)^{2N}}$$

$$\Rightarrow \frac{\epsilon^2}{A^2 - 1} = \left(\frac{\Omega_p}{\Omega_s} \right)^{2N}$$

Taking log on both sides,

$$2N \log \left(\frac{\Omega_p}{\Omega_s} \right) = \log \frac{\epsilon^2}{A^2 - 1}$$

$$N = \frac{1}{2} \log \left[\frac{\epsilon^2}{A^2 - 1} - \frac{\Omega_p}{\Omega_s} \right]$$

Case-II :- When specifications A_p , A_s , Ω_p and Ω_s are given

$$-A_p \leq |H(j\Omega)|_{dB} \leq 0$$

$$|H(j\Omega)|_{dB} \leq -A_s$$

At Ω_p ,

$$-A_p = 20 \log |H(j\Omega_p)|$$

At Ω_s ,

$$-A_s = 20 \log |H(j\Omega_s)|$$

$$\Rightarrow -A_p = 10 \log |H(j\omega_p)|^2$$

$$= 10 \log \left[\frac{1}{1 + \left(\frac{\omega_p}{\omega_c}\right)^{2N}} \right]$$

$$= 10 \log \left(\frac{1}{1 + \epsilon^2} \right)$$

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$$-A_s = 10 \log |H(j\omega_s)|^2$$

$$= 10 \log \left[\frac{1}{1 + \left(\frac{\omega_s}{\omega_c}\right)^{2N}} \right]$$

$$= 10 \log \left(\frac{1}{A^2} \right)$$

$$\left(\frac{\omega_p}{\omega_c} \right)^{2N} = 10^{A_p/10} - 1 \quad \text{--- (1)}$$

$$\left(\frac{\omega_s}{\omega_c} \right)^{2N} = 10^{A_s/10} - 1 \quad \text{--- (2)}$$

$$\left(\frac{\omega_p}{\omega_s} \right)^{2N} = \frac{10^{A_p/10} - 1}{10^{A_s/10} - 1}$$

$$2N \cdot \log \frac{\omega_p}{\omega_s} = \log \left[\frac{10^{A_p/10} - 1}{10^{A_s/10} - 1} \right]$$

find ω_c and N .

11th April, 19

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Ques. Determine the system function $H(s)$ for first order Butterworth filter.

$$|H(j\omega)|^2 = H(j\omega) \cdot H(-j\omega) = \frac{1}{1 + \left(\frac{\omega}{\omega_c}\right)^{2N}}$$

$$H(s) \cdot H(-s) = \frac{1}{1 + \left(\frac{-s^2}{\omega_c^2}\right)^N}$$

$$-s^{2N} + \omega_c^{2N} = 0$$

$$-s^{2N} = -\omega_c^{2N}$$

When N is even,

$$(-1)^N s^{2N} = e^{j(2k+1)\pi} \cdot \omega_c^{2N}$$

$$k = 0, \dots, (2N-1)$$

$$s^{2N} = e^{j(2k+1)\pi} \cdot \omega_c^{2N}$$

$$k = 0, \dots, (2N-1)$$

$$p_k = \omega_c \cdot e^{j\left(\frac{2k+1}{2N}\right)\pi}$$

$$-s^2 = -e^{j\left(\frac{2k+1}{2N}\right)\pi} \cdot \omega_c^{\frac{2N}{2N}} = \omega_c \cdot e^{j\frac{k\pi}{N}} \quad (\text{for } N \text{ is odd})$$

$$H(s) = \frac{\omega_c^N}{\prod (s - p_k)}$$

$$\underbrace{\quad}_{\text{only left-sided poles}}$$

only left-sided poles.

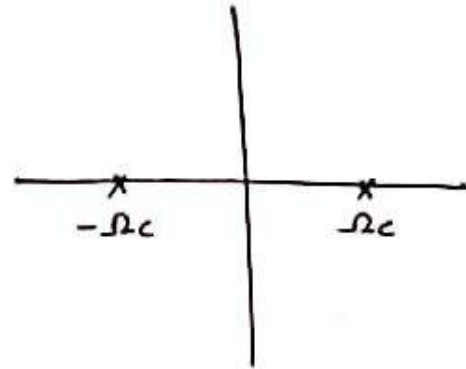
for odd N , in this question;

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$$P_k = \Omega_c \cdot e^{j \frac{k\pi}{N}}$$

$$P_1 = \Omega_c$$

$$P_2 = \Omega_c e^{j\pi} = -\Omega_c$$



the values of both the poles are real.

$$H(s) = \frac{\Omega_c}{[s - (-\Omega_c)]} = \frac{\Omega_c}{s + \Omega_c}$$

only the left pole

Ques: Determine the system function $H(s)$ for second order Butterworth filter.

order $n = 2$ i.e. $N \rightarrow$ Even.

$$S^{2N} = e^{j(2k+1)\pi} \cdot \Omega_c^{2N}$$

$$\Rightarrow P_k = \Omega_c \cdot e^{j\left(\frac{2k+1}{2N}\right)\pi}$$

$$= \Omega_c \cdot e^{j\left(\frac{2k\pi}{2N} + \frac{\pi}{2N}\right)}$$

$$= \Omega_c \cdot e^{j \frac{k\pi}{N}} \cdot e^{j \frac{\pi}{2N}}$$

$$= \Omega_c \cdot e^{j \frac{k\pi}{2}} \cdot e^{j \frac{\pi}{4}} = \Omega_c \cdot e^{j \left[\frac{(2k+1)\pi}{4} \right]}$$

$$p_1 = \Omega_c e^{j\pi/4} = (-0.707 + j0.707)\Omega_c$$

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$$p_2 = \Omega_c e^{j3\pi/4} = (-0.707 - j0.707)\Omega_c$$

$$p_3 = \Omega_c e^{j5\pi/4} = (0.707 - j0.707)\Omega_c$$

$$p_0 = \Omega_c e^{j\pi/4} = (0.707 + j0.707)\Omega_c$$

$$\therefore H(s) = \frac{\Omega_c^{2N}}{\prod (s - p_k)} = \frac{\Omega_c^{2N}}{(s - p_1)(s - p_2)}$$

$$H(s) = \frac{\Omega_c^{2(2)}}{(s - \Omega_c e^{j3\pi/4})(s - \Omega_c e^{j\pi/4})}$$

$\times p_1$	$\times p_0$
$\times p_2$	$\times p_3$

p_1 and p_2 are the conjugates of each other.

Ques. Compute the poles of an analog Butterworth filter that satisfies the conditions, 0.707

$$0.707 \leq |H(j\Omega)| \leq 1 \quad 0 \leq \Omega \leq 2$$

$$|H(j\Omega)| \leq 0.1 \quad \Omega \geq 4$$

Determine $H(s)$ and hence obtain $H(z)$ using Bilinear transformation assuming $T=1$.

Impulse Invariant

$$\Omega_p = \frac{\omega_p}{T}$$

$$\Omega_s = \frac{\omega_s}{T}$$

$$s = \frac{1}{T} \ln(z)$$

If we use Bilinear transformation -

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$$\Omega_p = \frac{2}{T} \tan\left(\frac{\omega_p}{2}\right)$$

$$\Omega_s = \frac{2}{T} \tan\left(\frac{\omega_s}{2}\right)$$

$$S = \frac{2}{T} \left(\frac{1-z^{-1}}{1+z^{-1}} \right)$$

$$\frac{1}{\sqrt{1+\epsilon^2}} \leq |H(j\Omega)| \leq 1$$

$$|H(j\Omega)| \leq \frac{1}{A}$$

p.e. $\Omega_p = 2$

$$\Omega_s = 4$$

$$\frac{1}{\sqrt{1+\epsilon^2}} = \frac{1}{\sqrt{2}}$$

$$\Rightarrow 1 + \epsilon^2 = 2$$

$$\Rightarrow \epsilon^2 = 1$$

$$\begin{cases} \epsilon = 1 \\ A = 10 \\ \Omega_p = 2 \\ \Omega_s = 4 \end{cases}$$

Case-I:-

$$N = \frac{1}{2} \log$$

$$N = \frac{\log\left(\frac{\epsilon^2}{A^2-1}\right)}{2 \log\left(\frac{\Omega_p}{\Omega_s}\right)}$$

$$= \log \left[\frac{\epsilon^2}{(A^2-1)} - \left(\frac{\Omega_p}{\Omega_s} \right)^2 \right]$$

$$= \log \left[\frac{1}{(100-1)} - \left(\frac{2}{4} \right)^2 \right]$$

$$= \log \left[\frac{1}{99} - \frac{1}{4} \right] = 3.31 \approx 4 \text{ (Even)}$$

$$\omega_c = \frac{\Omega_c}{2}$$

$$A^2 - 1 = \left(\frac{\Omega_s}{\Omega_c} \right)^{2N}$$

$$\Rightarrow 100 - 1 = \left(\frac{4}{\Omega_c} \right)^8$$

$$\Rightarrow 99 (\Omega_c)^8 = (4)^8$$

$$\Rightarrow \Omega_c = 2$$

k lies in between 0 to π

$$P_k = \Omega_c \cdot e^{j \left(\frac{2k+1}{2N} \right) \pi}$$

$$P_0 = 2 \cdot e^{j \frac{\pi}{8}} =$$

$$P_1 = 2 \cdot e^{j \frac{3\pi}{8}} =$$

$$P_2 = 2 \cdot e^{j \frac{5\pi}{8}} =$$

$$P_3 = 2 \cdot e^{j \frac{7\pi}{8}} =$$

$$P_4 = 2 \cdot e^{j \frac{9\pi}{8}} =$$

$$P_5 = 2 \cdot e^{j \frac{11\pi}{8}} = 2(-0.383 - 0.942j) \text{ left } \checkmark = P_2^* = 2e^{-j \frac{5\pi}{8}}$$

$$P_6 = 2 \cdot e^{j \frac{13\pi}{8}} = \text{right } \times$$

$$P_7 = 2 \cdot e^{j \frac{15\pi}{8}} = \text{right } \times$$

only poles on left-hand side are considered.

right \times

right \times

left \checkmark

left \checkmark

$$\text{left } \checkmark = P_3^* = 2e^{-j \frac{7\pi}{8}}$$

P_2 and P_5 are conjugates of each other.

and P_3 and P_4 are the conjugates of each other.

$$H(s) = \frac{\Omega_c^N}{(s-p_2) \cdot (s-p_3) \cdot (s-p_4) \cdot (s-p_5)}$$

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$$H(z) =$$

$$\text{put, } s = \frac{2}{T} \left(\frac{1-z^{-1}}{1+z^{-1}} \right)$$

12th April, 19

• Chebyshev :-

Chebyshev is all pole filter and types two is Poles and zero filter.

In type 1, magnitude response is equiripple in pass band and monotonic in stop band.

In type 2, it is monotonic in pass band and equiripple in stop band.

Type-2 is also called Inverse Chebyshev filter.

Advantage-

→ By choosing a filter that has an equiripple rather than a monotonic behaviour (Butterworth), we can obtain a lower order filter.

Magnitude filter response,

$$|H(j\omega)|^2 = \frac{1}{1 + \epsilon^2 T_N^2\left(\frac{\omega}{\omega_c}\right)}$$

where, $T_N(z)$ is the n^{th} order Chebyshev polynomial.

$$T_N(z) = \begin{cases} \cos(N \cos^{-1} z) & ; |z| \leq 1 \text{ Pass Band} \\ \cosh(N \cosh^{-1} z) & ; |z| > 1 \end{cases}$$

(1) $z=0$

$$|H(j\omega)|^2 = \frac{1}{1 + \epsilon^2 T_N^2(0)}$$

$$N=1, 2$$

$$T_1(0) = \cos(2/2) = 0$$

$$T_2(0) = \cos(2 \cdot 2/2) = 1$$

Even

$$|H(j\omega)|^2 = \frac{1}{1 + \epsilon^2}$$

Odd

$$|H(j\omega)|^2 = 1$$

(2) $z=1$

$$|H(j\omega_c)|^2 = \frac{1}{1 + \epsilon^2}$$

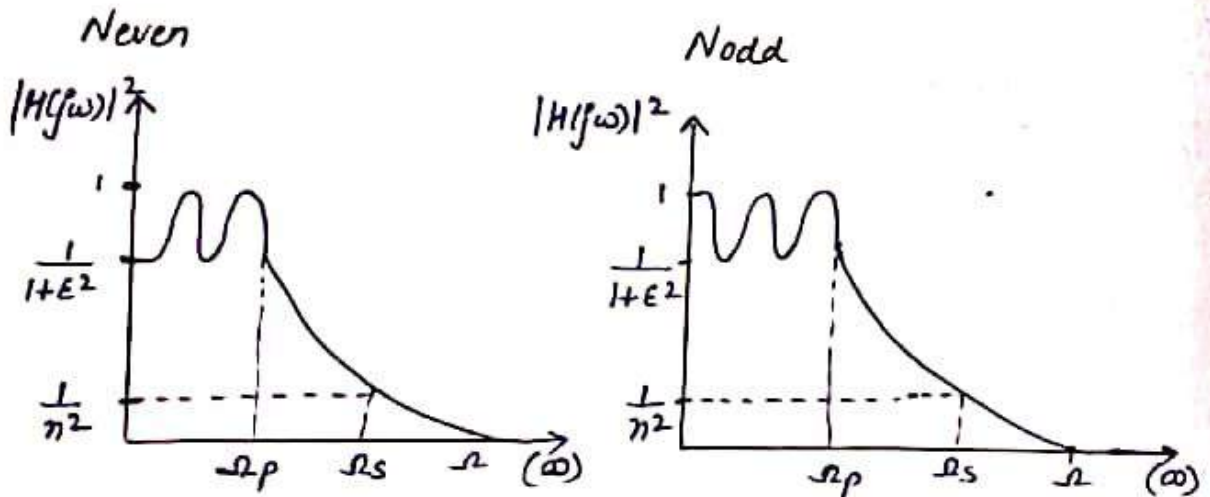
(3) $z > 1$

$$(\omega > \omega_c)$$

$$T_N(\infty) = \infty$$

$$|H(j^\circ\omega)|^2 = \frac{1}{1+\infty} = 0$$

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- Determination of filter parameters (N, Ω_c) of Cheby Shev filter -

Case I :- When specification $\epsilon, A, \Omega_p, \Omega_s$ are known -

$$|H(j^\circ\omega)^2| = \frac{1}{1 + \epsilon^2 T_N^2\left(\frac{\Omega}{\Omega_c}\right)}$$

General Specifications,

$$\frac{1}{1+\epsilon^2} \leq |H(j^\circ\omega)^2| \leq 1$$

$$|\Omega| \leq \Omega_c$$

$$|H(j^\circ\omega)^2| \leq \frac{1}{A^2}$$

(1) at $\Omega = \Omega_p$

$$|H(j^\circ\omega)|^2 = \frac{1}{1+\epsilon^2} = \frac{1}{1 + \epsilon^2 T_N^2\left(\frac{\Omega_p}{\Omega_c}\right)}$$

$$T_N\left(\frac{\Omega_p}{\Omega_c}\right) = 1$$

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$$\rightarrow T_N(1) = 1$$

$$\Rightarrow \left(\frac{\Omega_p}{\Omega_c}\right) = 1$$

(2) at $\Omega = \Omega_s$

$$|H(j\omega)|^2 = \frac{1}{A^2} = \frac{1}{1 + \epsilon^2 T_N^2\left(\frac{\Omega_s}{\Omega_c}\right)}$$

$$\epsilon^2 T_N^2\left(\frac{\Omega_s}{\Omega_c}\right) = A^2 - 1$$

$$T_N^2\left(\frac{\Omega_s}{\Omega_c}\right) = \frac{\sqrt{A^2 - 1}}{\epsilon}$$

$$\cosh\left(N \cosh^{-1} \frac{\Omega_s}{\Omega_c}\right) = \frac{\sqrt{A^2 - 1}}{\epsilon}$$

$$N = \frac{\cosh^{-1}(\sqrt{A^2 - 1} / \epsilon)}{\cosh^{-1}\left(\frac{\Omega_s}{\Omega_c}\right)}$$

Case-1:- When specifications A_p , A_s and Ω_p are known -

(1) When $\Omega = \Omega_p$

$$-A_p = 20 \log |H(j\omega)| = 10 \log |H(j\omega)|^2$$

$$= 10 \log \left(\frac{1}{1+\epsilon^2} \right)$$

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$$-A_p = 10 \log \frac{1}{1+\epsilon^2 T_N^2 \left(\frac{\Omega_p}{\Omega_c} \right)}$$

$$\boxed{-\Omega_p = -\Omega_c}$$

(2) At $\Omega = \Omega_s$

$$-A_s = 10 \log |H(j\Omega)|^2 = 10 \log \left(\frac{1}{A^2} \right)$$

$$-A_s = 10 \log \frac{1}{1+\epsilon^2 T_N^2 \left(\frac{\Omega_s}{\Omega_c} \right)} = 10 \log \frac{1}{A^2}$$

$$10^{-A_s/10} = \frac{1}{1+\epsilon^2 T_N^2 \left(\frac{\Omega_s}{\Omega_c} \right)}$$

$$\Rightarrow 1+\epsilon^2 T_N^2 \left(\frac{\Omega_s}{\Omega_c} \right) = 10^{A_s/10}$$

$$T_N^2 \left(\frac{\Omega_s}{\Omega_c} \right) = \frac{10^{A_s/10} - 1}{\epsilon^2} = \frac{10^{A_s/10} - 1}{10^{A_p/10} - 1}$$

$$T_N \left(\frac{\Omega_s}{\Omega_p} \right) = \frac{\sqrt{10^{A_s/10} - 1}}{\sqrt{10^{A_p/10} - 1}}$$

$$\cos h \left(N \cos h^{-1} \left(\frac{\Omega_s}{\Omega_c} \right) \right) = \sqrt{\frac{10^{A_s/10} - 1}{10^{A_p/10} - 1}}$$

$$N \cosh^{-1} \left(\frac{\Omega_s}{\Omega_c} \right) = \frac{\cosh^{-1} \sqrt{(10^{A_s/10} - 1) / (10^{A_p/10} - 1)}}{\cosh^{-1} (\Omega_s / \Omega_c)} \quad 136$$

Ques. Following are the specifications for a low pass filter, $\Omega_p = 1$ $A_p = 0.5 \text{ dB}$
 $\Omega_s = 2.33$ $A_s = 22 \text{ dB}$

Compute the filter order for Chebyshev Butterworth.

$$N = \frac{\cosh^{-1} \left(\sqrt{\frac{10^{22/10} - 1}{10^{-0.5/10} - 1}} \right)}{\cosh^{-1} (2.33)} = \frac{1.489}{1.489}$$

$N = 2.87$
 $N \approx 3$

also;

$$N = \frac{\log \left(\frac{\epsilon^2 / A^2 - 1}{2 \log \left(\frac{\Omega_p}{\Omega_s} \right)} \right)}{2 \log \left(\frac{\Omega_p}{\Omega_s} \right)} = \frac{-3.11}{-0.785}$$

$$N = 4.23 \approx 5$$

Type - 2 :- Che By Shev filter -

$$|H(j\omega)|^2 = \frac{1}{1 + \epsilon^2 \left[\frac{T_N^2(\Omega_s / \Omega_p)}{T_N^2(\Omega_s / \Omega_c)} \right]} = \frac{T_N^2(\Omega_s / \Omega_c)}{T_N^2(\Omega_s / \Omega_c) + \epsilon^2 T_N^2(\Omega_s / \Omega_p)}$$

$$\text{at } \Omega = 0$$

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$$|H(j\omega)|^2 = 1$$

$$\text{at } \Omega = \Omega_p$$

$$|H(j\omega)|^2 = \frac{1}{1+\epsilon^2}$$

$$\text{at } \Omega = \Omega_s$$

$$\frac{1}{1+\epsilon^2 T_N^2\left(\frac{\Omega_s}{\Omega_p}\right)} = \frac{1}{A^2}$$

$$\therefore N = \frac{\cosh^{-1}(\sqrt{A^2-1}/\epsilon)}{\cosh^{-1}(\Omega_s/\Omega_p)}$$

