Mewter-Raphson Method -

- 1) Facter Ivan Gauss-Seidal method of load flow
- 2) Its a powerful method for solving non-linear algebraic equ.

Corsider a set of n non-linear algebric equations.

fi(X) = 0 i=1,2,...h non-linear algebric equ.

$$X = \begin{cases} \alpha_1 \\ \alpha_2 \\ \vdots \\ \alpha_n \end{cases}$$

Lorresponding
$$\Delta \chi_1^0$$
corrections $\Delta \chi_1^0$

Algebric eque can se contren as - which are seen added to initial guess

$$f_i(x_1^2 + \Delta x_1^2, x_2^2 + \Delta x_2^2, \dots, x_n^2 + \Delta x_n^2) = 0$$
 $i = 1, 2, \dots$

so for all the equ., using Taylor series expension we can write

fi(xi, x2, -... xin) +
$$\frac{\partial f_i}{\partial x_i} |_{X=X^\circ} + \frac{\partial f_i}{\partial x_2} |_{X=X^\circ} + \frac{\partial f_i}{\partial x_2} |_{X=X^\circ} + \frac{\partial f_i}{\partial x_n} |_{X=X^\circ} + \frac{\partial f_$$

$$\begin{bmatrix}
\frac{\partial_{1}(x^{\circ})}{\partial x_{1}} \\ \frac{\partial_{1}}{\partial x_{1}} \\ \frac{\partial_{1}}{\partial x_{1}} \\ \frac{\partial_{1}}{\partial x_{1}} \\ \frac{\partial_{1}}{\partial x_{2}} \\ \frac{\partial_{1}}{\partial x_{$$

$$\begin{bmatrix}
d_{1}(x^{0}) \\
f_{2}(x^{0})
\end{bmatrix} + \begin{bmatrix}
\frac{\partial f_{1}}{\partial x_{1}} \\
\frac{\partial f_{2}}{\partial x_{1}} \\
\frac{\partial f_{2}}{\partial x_{2}} \\
\end{bmatrix}_{\chi_{2}\chi^{0}} \underbrace{\begin{bmatrix}
\frac{\partial f_{1}}{\partial x_{2}} \\
\frac{\partial f_{2}}{\partial x_{2}} \\
\frac{\partial f_{2$$

Staubian Matrix evaluated by taking Bertial derivative wind X(vector) & evaluated at X'

TTOTE O

$$\Delta X^{\circ} = \frac{-F^{\circ}}{J^{\circ}} = -[J^{\circ}]^{f} F^{\circ}$$

After X' = x°+ DX°

After the iteration
$$X^{r} = X^{r+1} + \Delta X^{r+1}$$

$$\Delta X^{r+1} = -\left[J^{r+1}J^{r}\right] + r^{r+1}$$

After putting values -

{t,(x), t2(x), --- tn(x)}

tolesance = Max {f, (x"), f_2(x") --- Jn (x")}

If tor < & (specified value)

Corresponding Xt

$$X_{\alpha^{2}} \left\{ \begin{array}{c} x^{\mu} \\ \vdots \\ x^{\lambda_{L}} \end{array} \right\}$$

These are

N-R method for load flow ?

Consider a power system having n-no. of Bus

est - dark Bus

2-7 - PQ BUS

Si = Pi+jai = Vi (E Tik Tik Vk)

Si=Pi-jai=Vi*T=Vi* FicVe

Vi = Vi (80

VK = VKLOK

Sit = Pi-jai = [Villie [Vik (Oir) [Vk (Or)]

= Vi = Tik / (100k+6k-60)

Q:=-V: Σ Yik Vk sin (Oik+6k-δi) - 2

10:2 f(8,V)

Let us introduce two functions
1) corresponding to a

$$\int_{t}^{\infty} = \Delta P_{t}^{0} = P_{t}^{1} - P_{t}^{1} \left(\delta_{2}, \delta_{3} - -\delta_{n}, V_{2}, V_{3} - V_{n} \right)$$

$$\text{springing} \quad \text{Includated value}$$

$$Virilian \quad \text{Includated value}$$

$$Virilian \quad \text{Include}$$

$$\int_{t}^{\infty} = \Delta P_{t}^{1} = P_{t}^{1} - P_{t}^{1} \left(\delta_{2}, \delta_{3} - -\delta_{n}, V_{2}, V_{3} - V_{n} \right)$$

$$\int_{t}^{\infty} = - \left[\int_{t}^{\infty} - P_{t}^{1} \left(\delta_{2}, \delta_{3} - -\delta_{n}, V_{2}, V_{3} - V_{n} \right) \right]$$

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$$\int_{t}^{\infty} =$$

$$\frac{\partial \Delta P_{i}^{2}}{\partial \delta_{j}} = \frac{\partial \left(P_{i}^{2} - P_{i}(\delta_{i}V)\right)}{\partial \delta_{j}}$$

$$\frac{\partial \Delta P_{i}^{2}}{\partial \delta_{j}} = \frac{\partial \left(P_{i}^{2} - P_{i}(\delta_{i}V)\right)}{\partial \delta_{j}}$$

$$\frac{\partial \Delta R_{i}}{\partial \delta_{j}} = \frac{\partial \left(P_{i}^{2} - Q_{i}(\delta_{i}V)\right)}{\partial \delta_{j}}$$

$$\frac{\partial \Delta R_{i}}{\partial \delta_{j}} = \frac{\partial \left(R_{i}^{2} - Q_{i}(\delta_{i}V)\right)}{\partial \delta_{j}}$$

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$$\frac{\partial \Delta R_{i}}{\partial \delta_{j}} = \frac{\partial R_{i}}{\partial \delta_{j}}$$

$$\frac{\partial R_{i}}{\partial \delta_{j}} = \frac{\partial R_{$$

$$\begin{aligned}
J_{21} &= \begin{bmatrix} \frac{\partial Q}{\partial \delta} \end{bmatrix} = \begin{bmatrix} \frac{\partial Q}{\partial \delta_{2}} & \frac{\partial Q}{\partial \delta_{3}} & -\frac{\partial Q}{\partial \delta_{n}} \\ \frac{\partial Q}{\partial \delta_{n}} & \frac{\partial Q}{\partial \delta_{n}} & -\frac{\partial Q}{\partial \delta_{n}} \\ \frac{\partial Q}{\partial \delta_{n}} & \frac{\partial Q}{\partial \delta_{n}} & -\frac{\partial Q}{\partial \delta_{n}} \\ \frac{\partial Q}{\partial \delta_{n}} & \frac{\partial Q}{\partial \delta_{n}} & -\frac{\partial Q}{\partial \delta_{n}} \end{bmatrix} \\
J_{22} &= \begin{bmatrix} \frac{\partial Q}{\partial V} \end{bmatrix} = \begin{bmatrix} \frac{\partial Q}{\partial V_{2}} & \frac{\partial Q}{\partial V_{2}} & -\frac{\partial Q}{\partial V_{n}} \\ \frac{\partial Q}{\partial V_{2}} & \frac{\partial Q}{\partial V_{2}} & -\frac{\partial Q}{\partial V_{n}} \\ \frac{\partial Q}{\partial V_{2}} & \frac{\partial Q}{\partial V_{2}} & -\frac{\partial Q}{\partial V_{n}} \end{bmatrix} \\
P_{i}^{c} &= V_{i} \sum_{k=1}^{N} Y_{ik}^{c} V_{k} cod \left[c_{ik} + \delta_{k} - \delta_{i}^{c} \right] \\
&= \frac{\partial Q}{\partial \delta_{i}^{c}} \begin{bmatrix} V_{i}^{c} \sum_{k=1}^{N} Y_{i}^{c} V_{k} cod \left[c_{ik} + \delta_{k} - \delta_{i}^{c} \right] \end{bmatrix} \\
&= \frac{\partial Q}{\partial \delta_{i}^{c}} \begin{bmatrix} V_{i}^{c} \sum_{k=1}^{N} Y_{i}^{c} cod \left[c_{ik} + \delta_{k} - \delta_{i}^{c} \right] + Y_{i}^{c} V_{2} cod \left[c_{ik} + \delta_{k} - \delta_{i}^{c} \right] + Y_{i}^{c} V_{2} cod \left[c_{ik} + \delta_{k} - \delta_{i}^{c} \right] + Y_{i}^{c} V_{2} cod \left[c_{ik} + \delta_{k} - \delta_{i}^{c} \right] \\
&= \frac{\partial Q}{\partial \delta_{i}^{c}} \begin{bmatrix} V_{i}^{c} \sum_{k=1}^{N} Y_{i}^{c} cod \left[c_{ik} + \delta_{i} - \delta_{i}^{c} \right] + Y_{i}^{c} V_{2} cod \left[c_{ik} + \delta_{k} - \delta_{i}^{c} \right] + Y_{i}^{c} V_{2} cod \left[c_{ik} + \delta_{k} - \delta_{i}^{c} \right] \\
&= V_{i}^{c} \left\{ c_{ik} + c_{ik} - c_{i}^{c} \right\} + V_{i}^{c} V_{2} cod \left[c_{ik} + \delta_{k} - \delta_{i}^{c} \right] \\
&= V_{i}^{c} \left\{ c_{ik} + c_{ik} - c_{i}^{c} \right\} + V_{i}^{c} V_{2} cod \left[c_{ik} + \delta_{k} - \delta_{i}^{c} \right] \\
&= V_{i}^{c} \left\{ c_{ik} + c_{ik} - c_{i}^{c} \right\} + V_{i}^{c} V_{2} cod \left[c_{ik} + c_{ik} - c_{i}^{c} \right] \\
&= V_{i}^{c} \left\{ c_{ik} + c_{ik} - c_{i}^{c} \right\} + V_{i}^{c} V_{2} cod \left[c_{ik} + c_{ik} - c_{i}^{c} \right] \\
&= V_{i}^{c} \left\{ c_{ik} + c_{ik} - c_{i}^{c} \right\} + V_{i}^{c} V_{2} cod \left[c_{ik} + c_{ik} - c_{i}^{c} \right] \\
&= V_{i}^{c} \left\{ c_{ik} + c_{ik} - c_{i}^{c} \right\} + V_{i}^{c} V_{2} cod \left[c_{ik} + c_{ik} - c_{i}^{c} \right] \\
&= V_{i}^{c} \left\{ c_{ik} + c_{ik} - c_{ik} - c_{ik}^{c} \right\} + V_{i}^{c} V_{2} cod \left[c_{ik} + c_{ik} - c_{i}^{c} \right] \\
&= V_{i}^{c} \left\{ c_{ik} + c_{ik} - c_{ik} - c_{ik}^{c} \right\} + V_{i}^{c} V_{2} cod \left[c_{ik} + c_{ik} - c_{ik}^{c} \right] \\
&= V_{i}^{c} \left\{ c_{ik} + c_{ik} - c_{ik} - c_{ik}^{c} \right\} + V_{i}^{c} \left\{ c_{$$

The deline of the property of = 3/6; Vi & Yi, us(0: +5,-6:)+YizV2 ws(0:2+62-6:)+-- - + Ti Vi Los (Dii+ 80-80) + -- -+ Tin Vn cos (oin = Vi { Yi, Visin (001+6,-6i) + Yi2 V2 sin(0; 2+ 62-6i) +---+0+YinVnsin(oin+8n-8i)} = Vi \(\sin \(\o ik + \delta_k - \dir \) = Vi \(\sin \(\text{Vic V \cent \(\text{Vic V \cen V \cent \(\text{Vic V \cent \(\text{Vic V \cent \(\text{Vic V \cent \(\text{V Ri - Yii Vi sin (Dii) Yir = Yii Ci 3Pi= - Qi - Vi2Bii = Y :: coso :: + j Y :: sin o :: = qii tj Bii J12 | 3Pi / 2 Vi Yij (a (Oij + Sj - Si)

$$\frac{\partial R_{i}}{\partial V_{i}} = \frac{P_{i}}{V_{i}} + V_{i} G_{i};$$

$$\frac{\partial R_{i}}{\partial S_{j}}\Big|_{i \neq j} = -V_{i} Y_{ij} V_{j} \cos(\sigma_{ij} + \delta_{j} - \delta_{i})$$

$$\frac{\partial R_{i}}{\partial S_{i}}\Big|_{i \neq j} = V_{i} \sum_{k=1}^{n} Y_{ik} V_{k} \cos(\sigma_{ik} + \delta_{k} - \delta_{i})$$

$$= V_{i} \sum_{k=1}^{n} Y_{ik} V_{k} \cos(\sigma_{ik} + \delta_{k} - \delta_{i}) - V_{i}^{2} Y_{ii} \cos(\sigma_{ii})$$

$$\frac{\partial R_{i}}{\partial S_{i}} = P_{i}^{2} - V_{i}^{2} G_{ii}$$

$$\frac{\partial R_{i}}{\partial V_{j}}\Big|_{i \neq j} = -V_{i} Y_{ij} \sum_{k=1}^{n} \sin(\sigma_{ij} + \delta_{j} - \delta_{i})$$

$$\frac{\partial R_{i}}{\partial V_{j}}\Big|_{i \neq j} = -\sum_{k=1}^{n} Y_{ik} V_{k} \sin(\sigma_{ik} + \delta_{i} - \delta_{i}) - V_{i} Y_{ii} \sin\sigma_{ii}$$

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$$\frac{\partial R_{i}}{\partial V_{j}}\Big|_{i \neq j} = -\sum_{k=1}^{n} Y_{ik} V_{k} \sin(\sigma_{ik} + \delta_{i} - \delta_{i})$$

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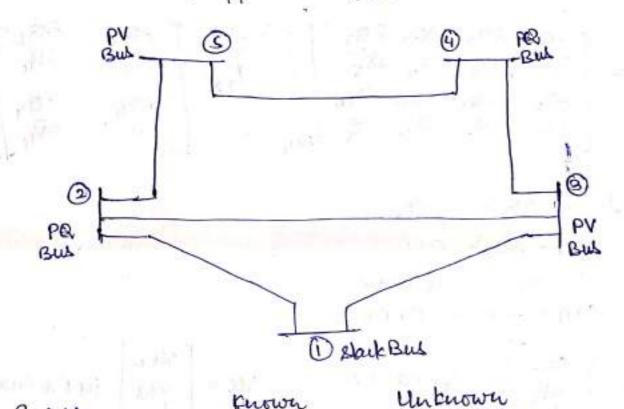
$$\frac{\partial R_{i}}{\partial V_{i}}\Big|_{i \neq j} = -\sum_{k=1}^{n} Y_{ik} V_{k} \sin(\sigma_{ik} + \delta_{i} - \delta_{i})$$

$$\frac{\partial R_{i}}{\partial V_{i}}\Big|_{i \neq j}$$

for PV Buses



- i) P is specified & i's not specified
- 3 AQ will not appear on LHS
- ii) V is specified OV will not appear on RHS



BILL NO.	(specifica)	(Non-specified)
2 (1-10)	P2R2	62V2
3	1 P3V3	63 Q3
4	Pu Qu	Sy Vy
5	P5 V5	Es As
ΔP2 ΔP2 ΔP3 ΔP4 ΔP5	DR= [DR2]	$\Delta 6 = \begin{bmatrix} \Delta C_2 \\ \Delta C_3 \\ \Delta C_4 \\ \Delta C_5 \end{bmatrix} \qquad \Delta V = \begin{bmatrix} \Delta V_2 \\ \Delta V_4 \end{bmatrix}$

$$J_{11} = \begin{bmatrix} \frac{\partial P_{12}}{\partial \delta_{2}} & \frac{\partial P_{2}}{\partial \delta_{1}} & \frac{\partial P_{2}}{\partial \delta_{2}} \\ \frac{\partial P_{3}}{\partial \delta_{2}} & \frac{\partial P_{3}}{\partial \delta_{1}} & \frac{\partial P_{3}}{\partial \delta_{2}} \\ \frac{\partial P_{3}}{\partial \delta_{2}} & \frac{\partial P_{3}}{\partial \delta_{3}} & \frac{\partial P_{3}}{\partial \delta_{4}} \\ \frac{\partial P_{3}}{\partial \delta_{2}} & \frac{\partial P_{3}}{\partial \delta_{3}} & \frac{\partial P_{3}}{\partial \delta_{4}} \\ \frac{\partial P_{3}}{\partial \delta_{2}} & \frac{\partial P_{3}}{\partial \delta_{3}} & \frac{\partial P_{4}}{\partial \delta_{4}} \\ \frac{\partial P_{3}}{\partial \delta_{2}} & \frac{\partial P_{4}}{\partial \delta_{3}} & \frac{\partial P_{4}}{\partial \delta_{4}} \\ \frac{\partial P_{3}}{\partial \delta_{2}} & \frac{\partial P_{4}}{\partial \delta_{3}} & \frac{\partial P_{4}}{\partial \delta_{4}} \\ \frac{\partial P_{3}}{\partial \delta_{2}} & \frac{\partial P_{4}}{\partial \delta_{3}} & \frac{\partial P_{4}}{\partial \delta_{4}} \\ \frac{\partial P_{3}}{\partial \delta_{2}} & \frac{\partial P_{4}}{\partial \delta_{3}} & \frac{\partial P_{4}}{\partial \delta_{4}} \\ \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{4}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} \\ \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4}}{\partial \delta_{5}} & \frac{\partial P_{4$$

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