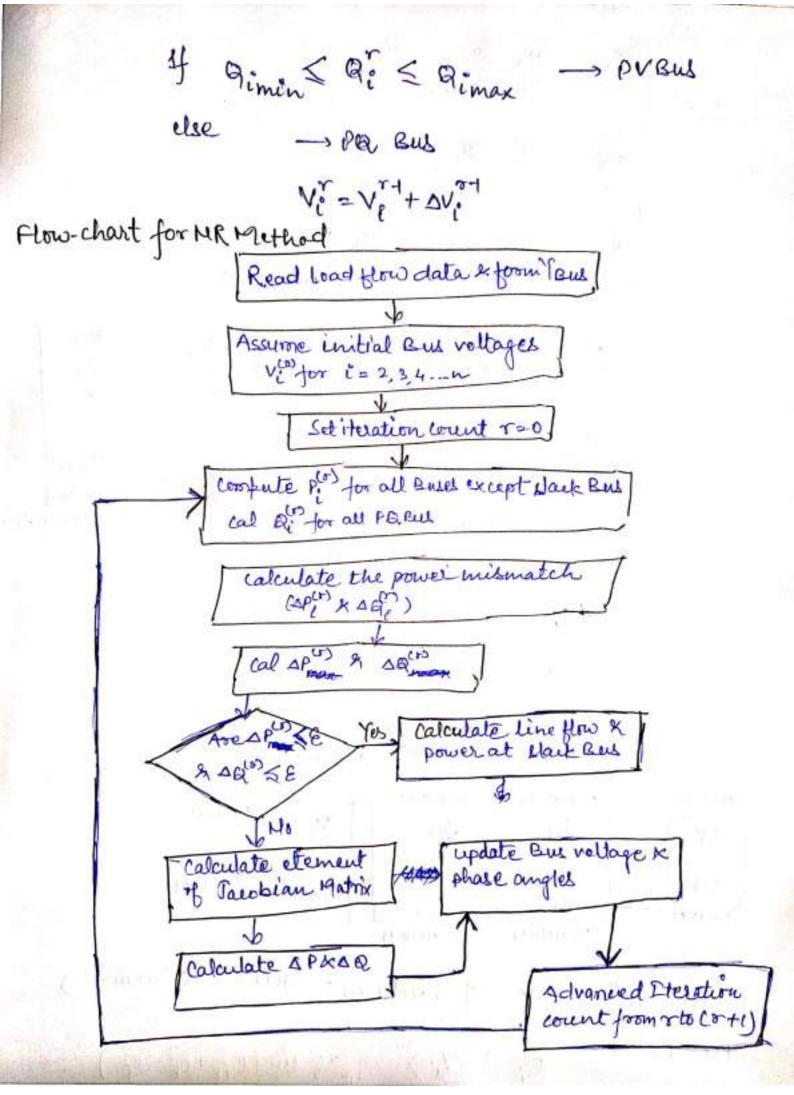
$$J_{11} = \begin{bmatrix} \frac{\partial P_2}{\partial N_2} & \frac{\partial P_1}{\partial \delta_m} & \frac{\partial P_1}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} \\ \frac{\partial P_2}{\partial \delta_m} & \frac{\partial P_2}{\partial \delta_m} &$$



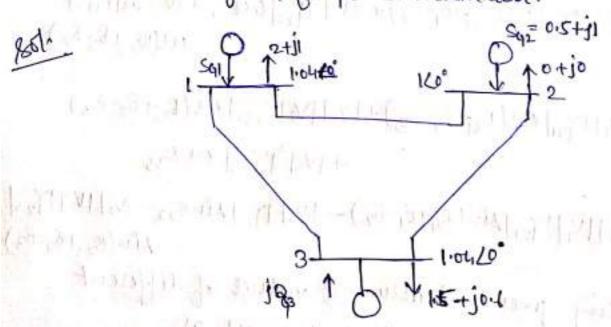
(37)

Each of the three Lines has a series impedance of 0.02+j0.08 pu and total should admittance of 0.02 pu. The specified quantities at the buses are tabulated below:

Bus	Real load Demand	Reactive Local Demand	Real Power	Reactive Power Gen.	Voltage specification
ı	2.0	1.0	Unspecified	unspaified	V,=1.04+jo
2_	0.0	0.0	0.5	1.0	unspecified (PR Bus)
3	in the	0.6	0· D	Q63= {	1/3/=1:04 pv Bus

Controllable reactive Power source is available at bus 3 with the constraint OSR43<1.5 pu.

Find the load flow solution using the NR method, Use a toleromice of 0.01 for power mismatch.



Using the nominal-to model for transmission lines, You for the given system is obtained at follows: For each line

Fresia = 1 - 2.941-j11.764 = 12.18 - 75.96°

Each off-diagonal term = - 2.941+j11.764

Each self team = 2[12,941-j11.764)+j0.01]

= 24.23/-75.95°

TBW2 [36/23/2436] 12-13/14-04 [12-13/14-04] [2-13/14-04] [2-13/14-04] 12-13/14-04] 12-13/14-04]

To start iteration choose 12= 1+jo 9 83=0

P2= 1/2/1/1/1/2/ cos(02+6,-62)+ 1/2/1/2/ cos022+1/2/1/2/ cos(023+63-62)

P32 [V3] [V1] [Y31] cos (03 + 6, -62) + 1 V3 [[V2] [Y32] cos (032+62-63) + 1 V3 [Y33] cos 033

substituting given and assumed values of different quantities, we get the values of powers as

Power Residuals

$$\Delta P_2^2 = P_2^8 - P_2^8$$

$$= 0.5 - (-0.24) = 0.73$$

changes in variables at the end of the first iteration are

obtained as
$$\begin{bmatrix} \frac{\partial P_2}{\partial \delta_2} & \frac{\partial P_2}{\partial \delta_3} & \frac{\partial P_2}{\partial N_24} \\ \Delta P_3 \\ \Delta P_3 \\ \Delta Q_2 \end{bmatrix} = \begin{bmatrix} \frac{\partial P_2}{\partial \delta_2} & \frac{\partial P_3}{\partial \delta_3} & \frac{\partial P_3}{\partial N_24} \\ \frac{\partial P_3}{\partial \delta_2} & \frac{\partial P_3}{\partial \delta_3} & \frac{\partial P_3}{\partial N_24} \\ \frac{\partial Q_2}{\partial \delta_2} & \frac{\partial Q_2}{\partial \delta_3} & \frac{\partial Q_2}{\partial N_24} \end{bmatrix} \begin{bmatrix} \Delta \delta_2 \\ \Delta \delta_3 \\ \Delta N_2 \end{bmatrix}$$

Jacobian melements can be evaluated by differentiating the expressions given above for P2, P3, Q2 w.r.t. S2, S3 x [v2]

$$\begin{bmatrix} \Delta \delta_{1}^{2} \\ \Delta \delta_{3}^{2} \\ \Delta \delta_{3}^{2} \end{bmatrix} = \begin{bmatrix} 24.47 & -12.23 & 5.64 \\ -12.23 & 24.95 & -3.65 \\ -6.11 & 3.05 & 22.94 \end{bmatrix} \begin{bmatrix} 6.73 \\ -1.62 \\ 1.96 \end{bmatrix} = \begin{bmatrix} -6.023 \\ -0.089 \end{bmatrix}$$

$$\begin{bmatrix} \delta_{2}^{1} \\ \delta_{3}^{2} \\ 1 V_{2}^{1} \end{bmatrix} = \begin{bmatrix} \delta_{2}^{0} \\ \delta_{3}^{2} \\ 1 V_{2}^{1} \end{bmatrix} + \begin{bmatrix} \Delta \delta_{2}^{1} \\ \Delta \delta_{3}^{1} \\ \Delta V_{2}^{1} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} + \begin{bmatrix} -6.023 \\ -0.0694 \\ 0.089 \end{bmatrix} = \begin{bmatrix} -0.023 \\ -0.0694 \\ 1.089 \end{bmatrix}$$

$$\begin{cases} \delta_{3}^{1} \\ 1 V_{2}^{1} \end{bmatrix} = \begin{bmatrix} 0 \\ 1 \end{bmatrix} + \begin{bmatrix} -6.023 \\ -0.0694 \\ 0.089 \end{bmatrix} = \begin{bmatrix} -0.023 \\ -0.0694 \\ 1.089 \end{bmatrix}$$

$$\begin{cases} \delta_{3}^{1} \\ 1 V_{2}^{1} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} + \begin{bmatrix} -6.023 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} -0.023 \\ -0.0694 \\ 1.089 \end{bmatrix}$$

$$\begin{cases} \delta_{3}^{1} \\ 1 V_{2}^{1} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} + \begin{bmatrix} -6.023 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} -0.023 \\ -0.0694 \\ 1.089 \end{bmatrix}$$

$$\begin{cases} \delta_{3}^{1} \\ 1 V_{2}^{1} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} -6.023 \\ 0 \end{bmatrix} = \begin{bmatrix} -0.023 \\ -0.0694 \\ 1.089 \end{bmatrix}$$

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$$\begin{cases} \delta_{3}^{1} \\ 1 V_{2}^{1} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} + \begin{bmatrix} -6.023 \\ 0 \end{bmatrix} = \begin{bmatrix} -0.023 \\ 0 \end{bmatrix} = \begin{bmatrix} -0.023 \\ 0 \end{bmatrix}$$

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$$\begin{cases} \delta_{3}^{1} \\ 1 V_{2}^{1} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} + \begin{bmatrix} -6.023 \\ 0 \end{bmatrix} = \begin{bmatrix} -0.023 \\ 0 \end{bmatrix} = \begin{bmatrix} -0.023 \\ 0 \end{bmatrix}$$

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